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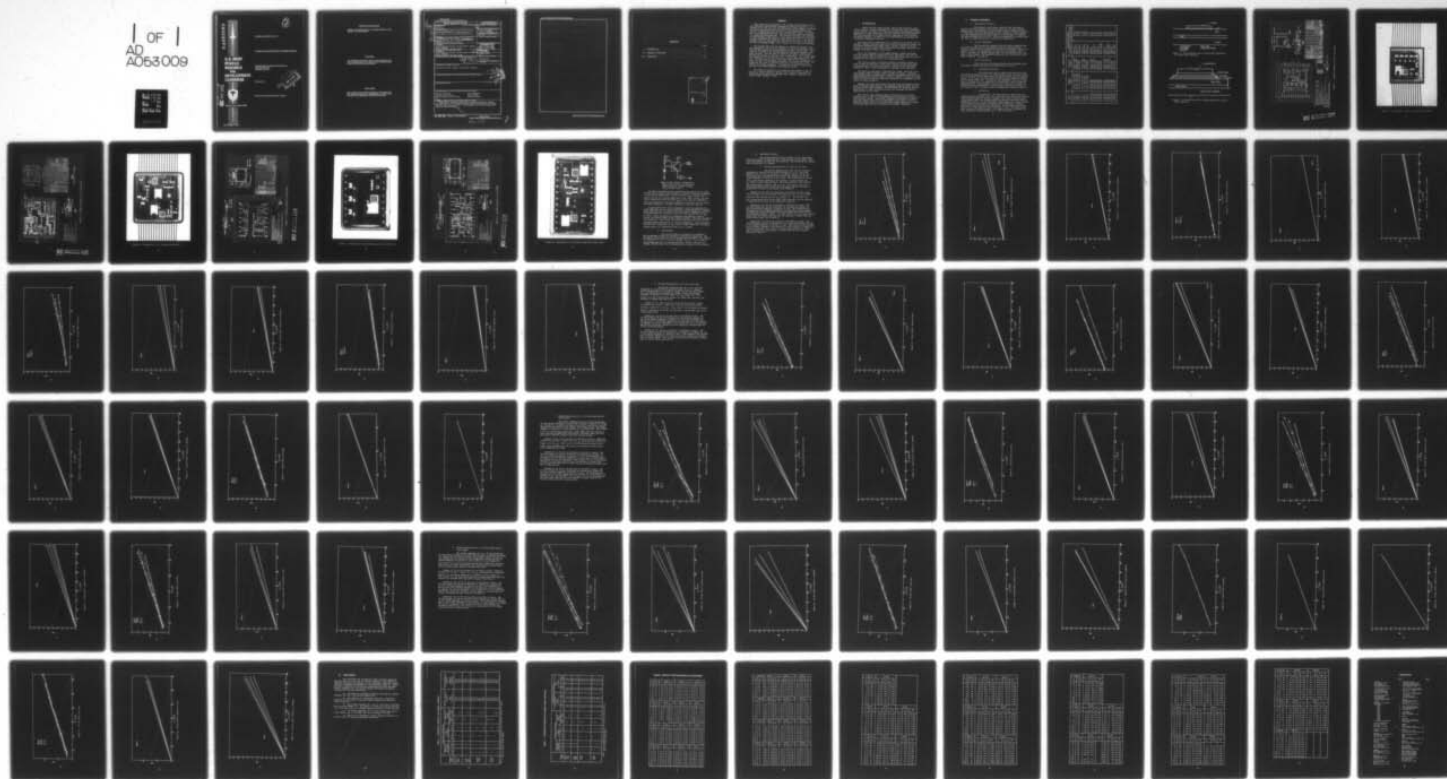
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THERMAL CHARACTERISTICS OF HYBRID CIRCUITS.(U)  
MAY 77 J AGOSTA, S G DAS, R RIBBE, C E RILEY

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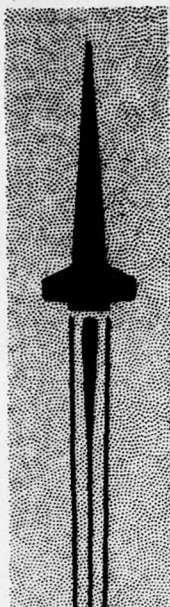


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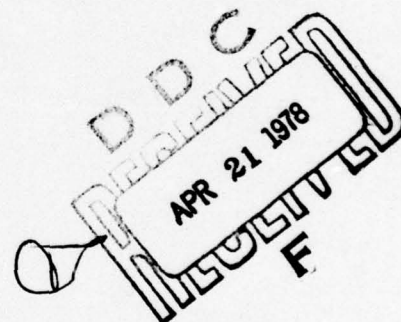
**U.S. ARMY  
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TECHNICAL REPORT EA-77-1

THERMAL CHARACTERISTICS OF HYBRID CIRCUITS

Advanced Systems Development and Manufacturing  
Technology Directorate  
Engineering Laboratory

12 May 1977



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| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number)<br>This report presents an evaluation of thermal resistance in hybrid microelectronics. Four different package types were used with and without multiple layer thick circuitry. Chip components were attached using both epoxy and eutectic methods. |  |   |

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# Summary

This report is an evaluation of the thermal characteristics of new and different microelectronic packages and assembly techniques. The packages are of the lead gull and double-lead in-line design. The mounting of the semiconductor die is done with the standard gold-epoxy eutectic technique and with the use of a gold filled epoxy. The latter technique is an additional dielectric and gold conductor layer was deposited to a single gold metallization. The substrate attachment was performed by epoxy bonding using either a silver filled resin (R-41V) or an ultra-thermally conductive and thermally conductive epoxy (R-74). The thermal impedance from the junction to the ambient for the packages was determined with the package fitted into a hole of a p-board was evaluated.

## CONTENTS

|                                    | Page |
|------------------------------------|------|
| I. INTRODUCTION . . . . .          | 3    |
| II. TECHNICAL DISCUSSION . . . . . | 4    |
| III. CONCLUSIONS . . . . .         | 68   |

The recorded data were the ambient air temperature, the package temperature, the power dissipation, and the thermal impedance. The data were recorded for each package type and for each assembly technique. The thermal impedance was determined by the power dissipation and the temperature difference between the junction and the ambient. The thermal impedance was determined by the power dissipation and the temperature difference between the junction and the ambient.

The report is intended to be an important development of the end user for a selected group of variables and therefore correlated by a comparison with industry packages type, assembly techniques, and actual thermal impedance values.

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## SUMMARY

This report is an evaluation of the thermal characteristics of several different microelectronic packages and assembly techniques. The packages are of the flat pack and double-dual in-line design. The mounting of the semiconductor die is done with the standard gold-silicon eutectic technique and with the use of a gold filled epoxy. The influence of an additional dielectric and gold conductor layer was compared to a simple gold metallization. The substrate attachment was performed by epoxy mounting using either a silver filled resin (H-417) or an electrically insulative and thermally conductive epoxy (H-74). The thermal impedance from the junction to the case and the junction to the static air with the package plugged into a socket of a p-c board was evaluated.

The recorded data were the ambient air temperature (preset), the case temperature, and the power necessary to raise the junction to 175°C. The data were graphed as the temperature difference versus power. The slope of the graph is the thermal impedance expressed in degrees centigrade per Watt. The data were recorded for any offsets due to self-heating and averaged to constant value if applicable. The thermal impedance expressed as a constant for each of the packaged types of 3/4- and 1-in. flat packs and 16- and 24-pin double-dual in-line packages is given for each of the assembly techniques. The greater the thermal path length and the lower the thermal conductivity of the material, the greater the thermal impedance. The larger the package's surface area, the lower the thermal impedance from junction to air.

The report is intended to be an empirical development of the subject for a selected group of variables and therefore correlated by a comparison matrix indicating packages type, assembly techniques, and actual thermal impedance values.



## I. INTRODUCTION

Modern military system designs require high-reliability electronic circuits. Present techniques for insuring that these requirements are met include the limitation of maximum allowable semiconductor junction temperatures to some value lower than that specified by the manufacturer. With the increasing use of hybrid circuit technology in these systems, the hybrid designer is charged with the responsibility of insuring that reliability requirements are met.

Operating junction temperatures are a function of the device and its package. Thermal resistance values for discrete semiconductor devices can be readily determined from simple tests. However, thermal resistance figures for various hybrid circuit fabrication techniques, materials, and packages have been, at best, a gray area.

Due to the uniqueness of most hybrid designs, thermal resistance data and maximum junction temperatures to be experienced could only be estimated within  $\pm 20\%$  from tables of thermal conductivity for the materials involved and data sheets of the active components used.

This report provides information needed by the hybrid designer in order to make calculations to within  $\pm 5\%$ , thereby allowing intelligent design tradeoffs to be made with respect to materials and fabrication techniques. Thus, costly overdesigns or redesigns can be minimized.

The study was undertaken to determine the thermal resistance variations brought about by several common assembly techniques. Variables investigated include package styles, substrate attachment materials, chip bonding techniques, and multilayer circuitry (typical of analog circuitry). Thick film test circuits were specially fabricated for measurement of the effects of these variables.

Thermal resistance calculations were made using strategically placed power dissipating semiconductors and temperature sensors inside the hermetically sealed hybrid packages. New techniques for measuring junction temperature of a power dissipating device were developed and used to generate data for the study.

Test results show comparable detailed thermal data for various assembly plans in light of the maximum junction temperature allowed in a hybrid circuit design. Measurement techniques are discussed in detail such that further study can be accomplished by the reader in order to generate thermal data for his own particular hybrid application, including package types, specific materials, and assembly techniques.

## II. TECHNICAL DISCUSSION

### A. Experimental Procedure

This section of the report identifies the technique by which the thermal impedance data were generated for the four different package types. The circuits were built with standard assembly techniques, the data were derived by maintaining the test chamber at a given temperature and supplying sufficient power (Watts) to the package to stabilize the junction temperature at 175°C. The case temperature was recorded when the total package configuration stabilized in temperature.

### B. Circuit Preparation

The circuits were prepared with the typical manufacturing and assembly techniques used throughout the hybrid microelectronic industry. Figures 1 and 2 present the typical cross-sectional views of the hybrid circuits. The thicknesses are also listed in Figures 1 and 2. Table 1 indicates the package bonding types and corresponding serial numbers of the circuits. The assembly drawing and view of the circuits are shown in Figures 3 through 10.

### C. Circuit Evaluation

This section of the report describes the techniques which were used to measure and analyze the manufactured circuits.

#### 1. Measurement Technique

The transistors used for power dissipators were used with constant current sources. The zener diodes and all resistors needed for the constant current sources were outside the hybrid and were discrete parts. In this way, the only device dissipating power inside the hybrid was the device under test. In addition, the calibration current was kept small with respect to the capability of the particular chip to minimize heating effects. Where possible, silicon diodes were used to verify and measure substrate temperature at various points and were calibrated, in this case, at 1 mA. A typical circuit configuration is shown in Figure 11.

#### 2. Calibration

The junction to be used (sensor or dissipator) was calibrated before the power run. All transistors were set up with constant current sources using the same base voltage as was used for actual tests. A test chamber which was nitrogen cooled and electric heated was used for temperature control. An iron/constantan thermocouple, in intimate contact with the bottom of the header, monitored header temperature; a similar thermocouple monitored the oven temperature. The reference junction was mounted in a large aluminum block maintained at 72°F. The thermocouples were initially calibrated against a lab standard digital thermometer and were periodically checked during the running of the tests.

TABLE 1. SAMPLE DESIGN

| Serial No. | Package Type      | Substrate Design | Bonding Techniques |                |
|------------|-------------------|------------------|--------------------|----------------|
|            |                   |                  | Die Attach         | Substrate Bond |
| H 215-3    | 3/4-in. Flat Pack | Single layer     | Eutectic           | H-417          |
| H 215-4    | 3/4-in. Flat Pack | Single layer     | Epoxy (A41)        | H-417          |
| H 215-1    | 3/4-in. Flat Pack | Multilayer       | Eutectic           | H-417          |
| H 215-2    | 3/4-in. Flat Pack | Multilayer       | Epoxy (H41)        | H-417          |
| H 214-3    | 1-in. Flat Pack   | Single layer     | Eutectic           | H-417          |
| H 214-4    | 1-in. Flat Pack   | Single layer     | Epoxy (H41)        | H-417          |
| H 214-1    | 1-in. Flat Pack   | Multilayer       | Eutectic           | H-417          |
| H 214-2    | 1-in. Flat Pack   | Multilayer       | Epoxy (H41)        | H-417          |
| H 217-3A   | 16-Pin DDIL       | Single layer     | Eutectic           | H-74           |
| H 217-3B   | 16-Pin DDIL       | Single layer     | Eutectic           | H-417          |
| H 217-4A   | 16-Pin DDIL       | Single layer     | Epoxy (H41)        | H-74           |
| H 217-1A   | 16-Pin DDIL       | Multilayer       | Eutectic           | H-74           |
| H 217-1A   | 16-Pin DDIL       | Multilayer       | Eutectic           | H-417          |
| H 217-2B   | 16-Pin DDIL       | Multilayer       | Epoxy (H-41)       | H-74           |
| H 217-2B   | 16-Pin DDIL       | Multilayer       | Epoxy (H-41)       | H-417          |
| H 216-3A   | 24-Pin DDIL       | Single layer     | Eutectic           | H-74           |
| H 216-3B   | 24-Pin DDIL       | Single layer     | Eutectic           | H-417          |
| H 216-4A   | 24-Pin DDIL       | Single layer     | Epoxy (H41)        | H-74           |
| H 216-4B   | 24-Pin DDIL       | Single layer     | Epoxy (H41)        | H-417          |
| H 216-1B   | 24-Pin DDIL       | Multilayer       | Eutectic           | H-417          |
| H 216-2A   | 24-Pin DDIL       | Multilayer       | Epoxy (H41)        | H-74           |
| H 216-2B   | 24-Pin DDIL       | Multilayer       | Epoxy (H41)        | H-417          |



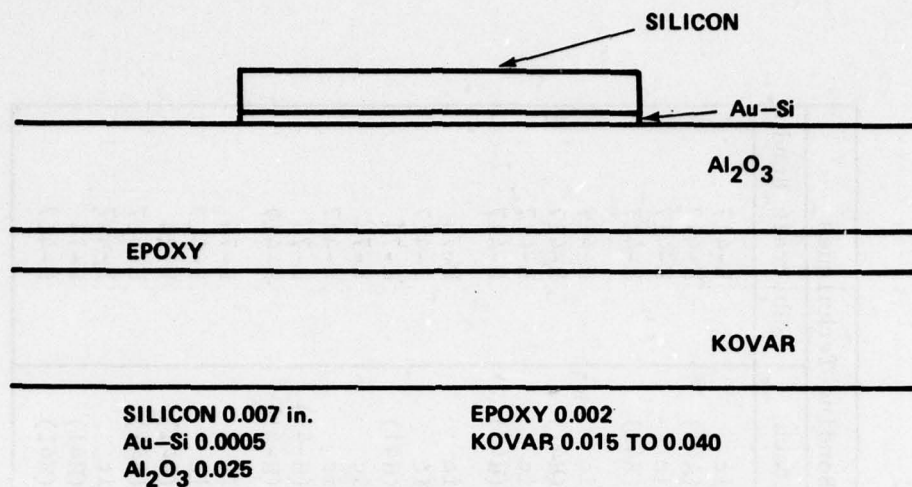


Figure 1. Cross-sectional view of eutectically mounted die on single layer substrate.

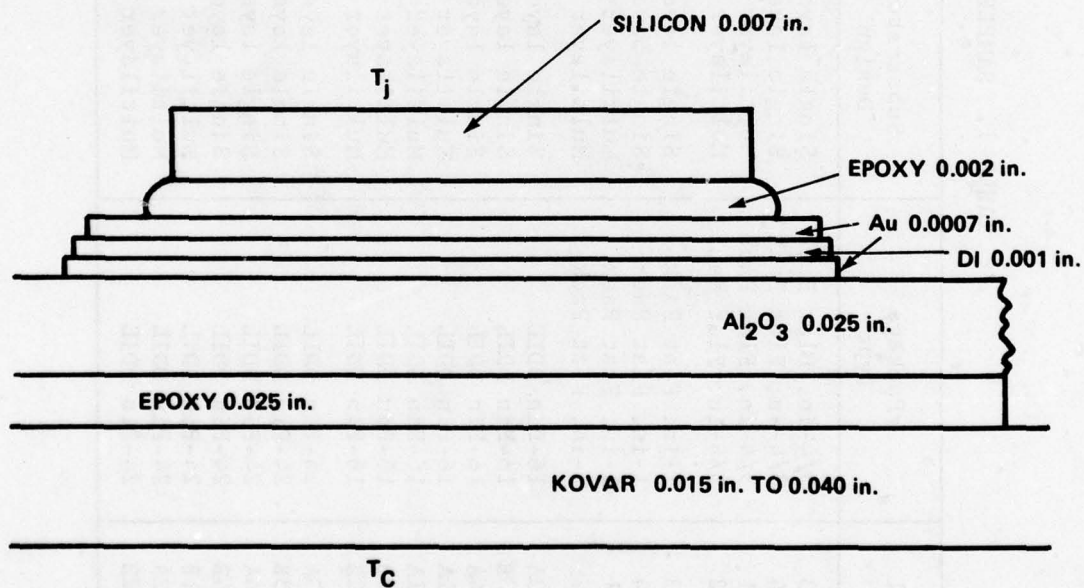


Figure 2. Cross-sectional view of epoxy mounted die on multi-layer substrate.



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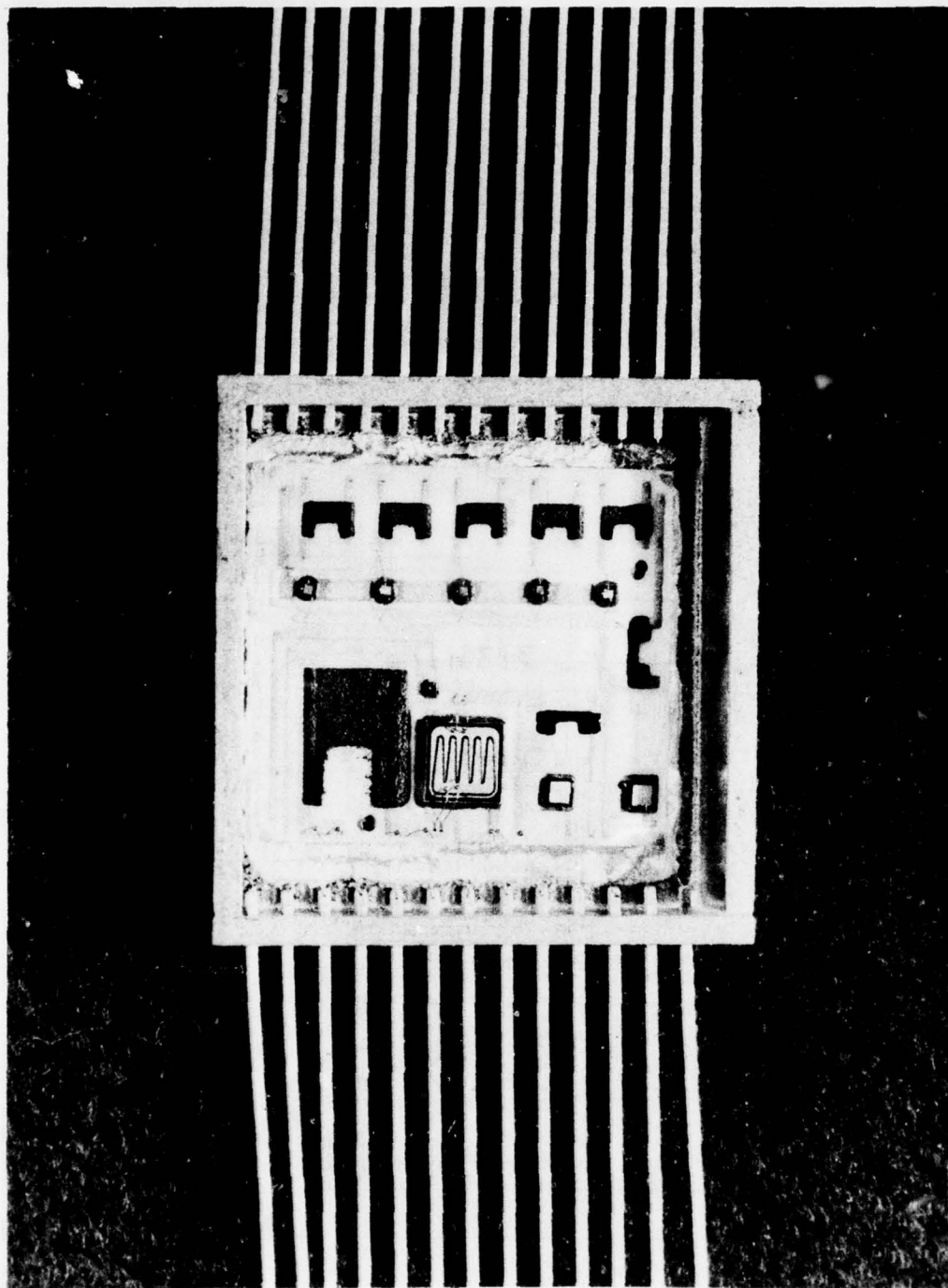
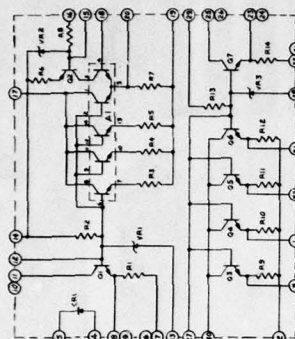
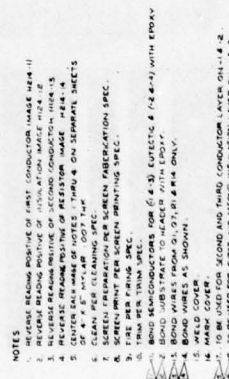


Figure 4. Photograph of 3/4-in. flat pack circuit H215.





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Figure 5. Assembly drawing of 1-in. flat pack.

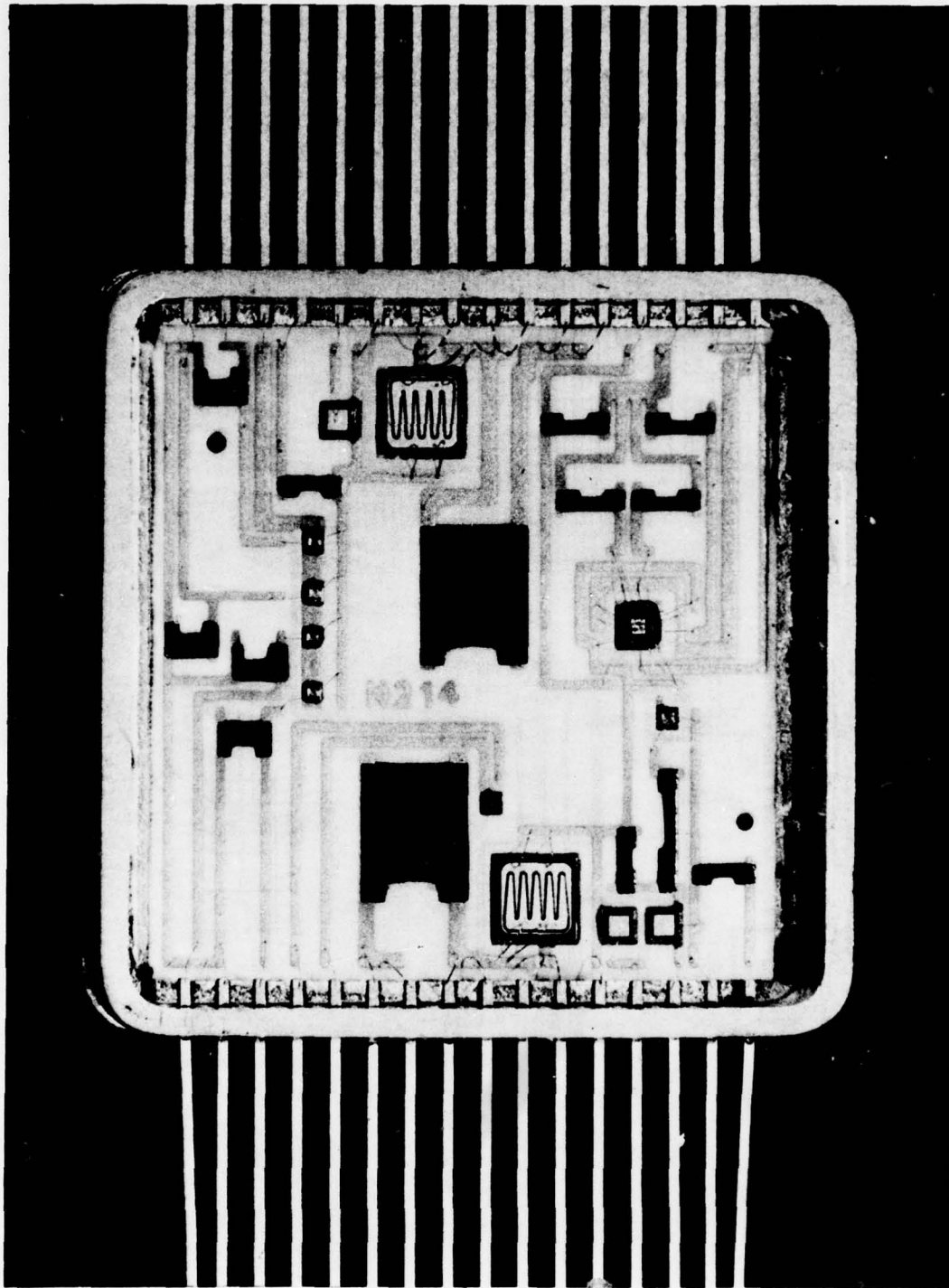


Figure 6. Photograph of 1-in. flat pack circuit H214.

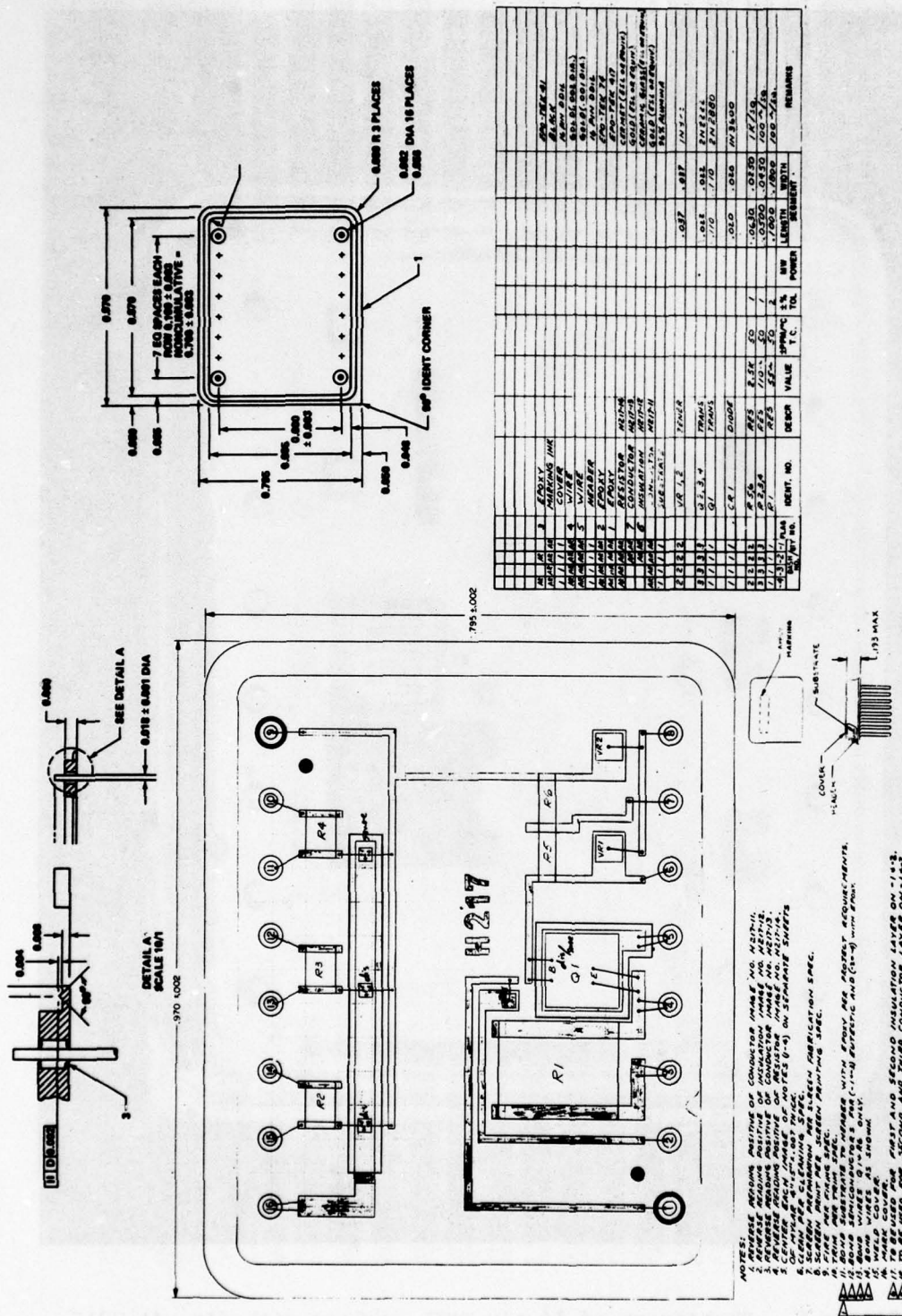


Figure 7. Assembly drawing of 16-pin DDIL.

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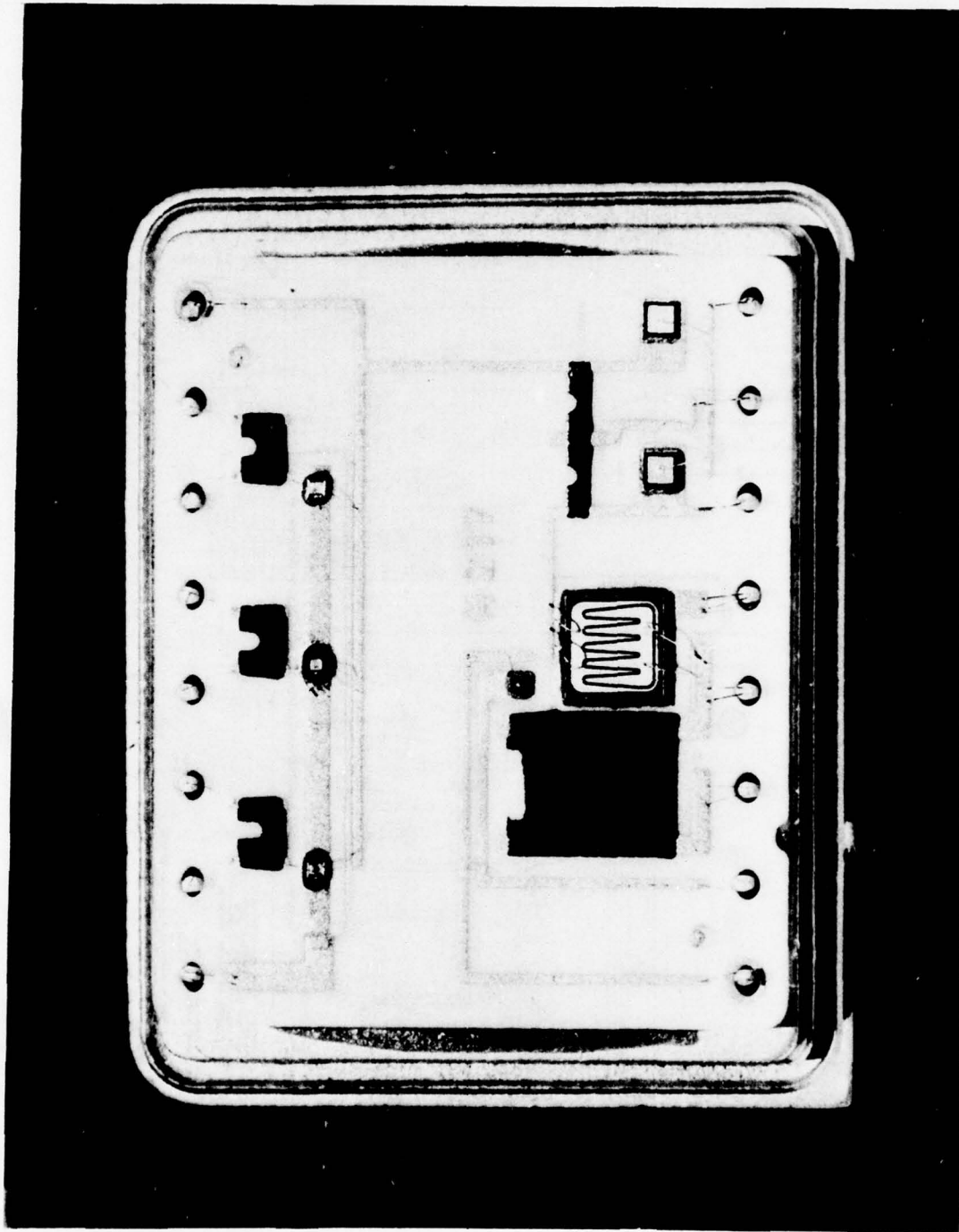


Figure 8. Photograph of 16-pin DDIL package with circuit H217.



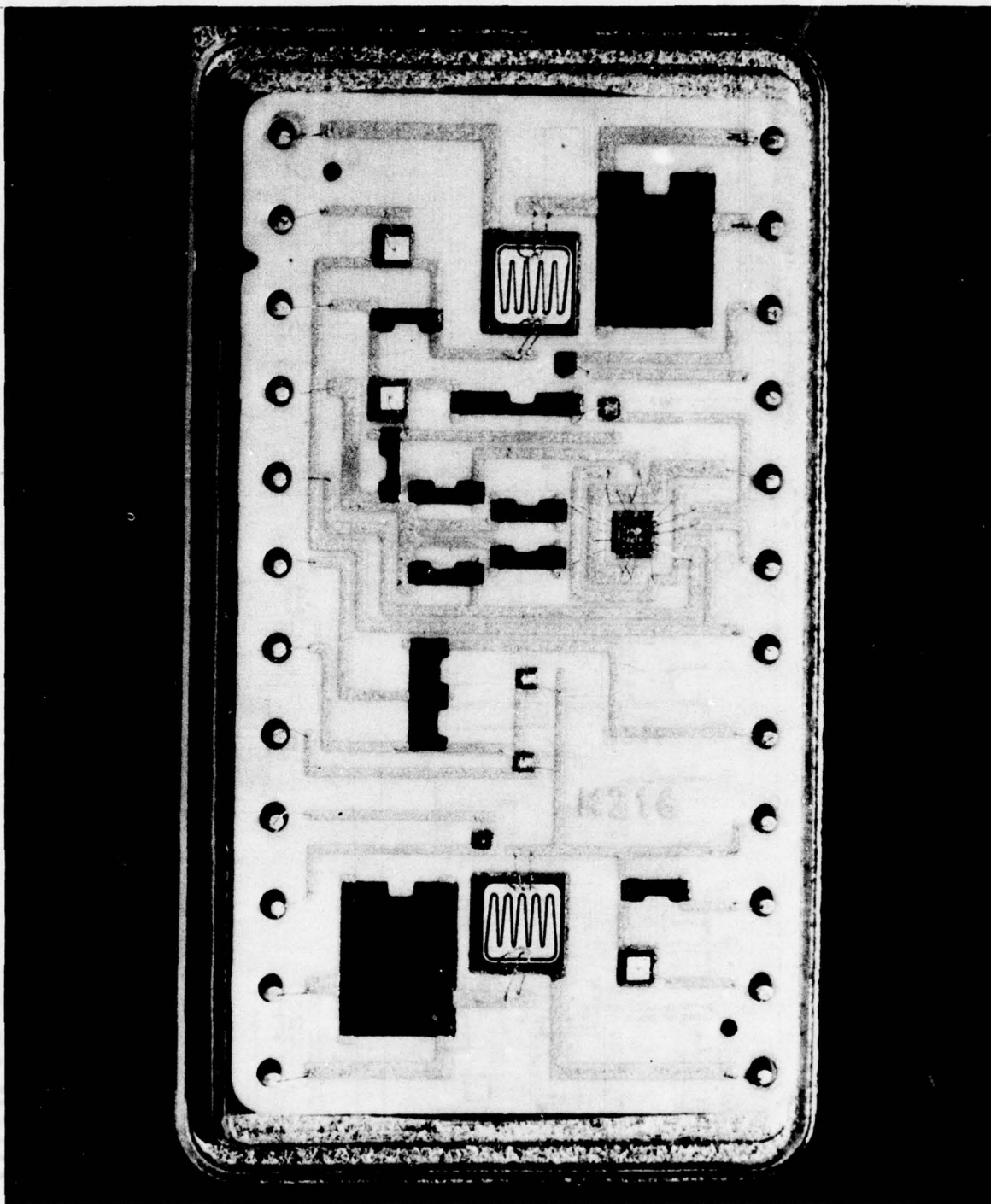


Figure 10. Photograph of 24-pin DDIL package with circuit H216.



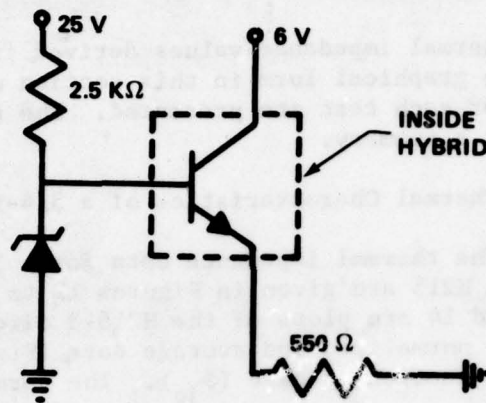


Figure 11 Test circuit configuration.  
(The 2.5 kΩ resistor and zener were substituted by a constant voltage source in most tests.)

The basic technique used for calibrating the junction was to apply the base and collector voltage (Figure 11) and then stabilize the package at the required temperature, read and record the  $V_{BE}$  (voltage base to emitter) at all the required temperatures from  $-55^{\circ}\text{C}$  to  $150^{\circ}\text{C}$ , and then draw a calibration curve from which  $V_{BE}$  at  $175^{\circ}\text{C}$  junction temperature could be interpolated. The power dissipated during this test was always very small compared to the power capability of the chip involved.

It was decided that junction temperature would be maintained at a fixed temperature for all tests; therefore, a given package was installed in the oven, the oven was stabilized at the required temperature, and the collector voltage was increased to the point that  $V_{BE}$  equalled the  $V_{BE}$  at  $175^{\circ}\text{C}$ . Power dissipation was computed by multiplying collector current (a constant) times collector-emitter voltage. The power dissipation was recorded on a chart along with header temperature and the  $V_f$  of any reference diodes available on the substrate (Appendix). This information allowed direct computation of  $\theta_{jc}$  as well as power capability of a given package type at all temperatures from  $-55^{\circ}\text{C}$  to  $+150^{\circ}\text{C}$ .

### 3. Data Analysis

All raw data taken are provided in the Appendix. The thermocouple voltage was converted to equivalent temperature. The wattage per device and total for the package was calculated. The junction was maintained at  $175^{\circ}\text{C}$ . A plot of wattage versus  $T_j - T_c$  was made on each package type and each bonding technique. Table 1 indicates the package, bonding types, and corresponding serial numbers of the circuits.

#### D. Experimental Results

The thermal impedance values derived from the experimental data are presented in graphical form in this section of the report. The actual data points for each test are presented. The normalized and average data are presented as a summary.

##### 1. Thermal Characteristics of a 3/4-in. Flat Pack

The thermal impedance data for a 3/4-in. flat-pack designated as circuit H215 are given in Figures 12 to 23. The first Figures of 12, 13, and 14 are plots of the H215-3 circuit for the raw data (Figure 12), the normalized and average data (Figure 13) of the thermal impedance of junction to case ( $\theta_{jc}$ ). The normalized and average data of the thermal impedance of the junction to static ambient air  $\theta_{ja}$  (Figure 14) are also presented. The three different lines indicate the three packages analyzed. (SN 7, 8, 9). This circuit (-3) was a eutectically mounted die, single layer substrate with the substrate to header bond via silver filled epoxy, H-417 (Table 1).

Figures 15, 16, and 17 are the plots of the H215-4 circuit. The raw data (Figure 15) and averaged data (Figure 16) for  $\theta_{jc}$  are provided along with the averaged data for  $\theta_{ja}$  (Figure 17). This circuit (-4) was an epoxy mounted die (H-41) single layer substrate with the substrate to header bond via silver filled epoxy H417 (Table 1).

Figures 18, 19, and 20 are the plots of the H215-1 circuit. The raw data (Figure 18) and the normalized and averaged data (Figure 19) are of the thermal impedance of junction to case. The normalized and averaged data of the thermal impedance of the junction to static ambient air (Figure 20) are also presented. The three different lines indicate the three packages analyzed. (SN 1, 2, 3) this circuit (-1) was a eutectically mounted die, multilayer substrate with the substrate to header bond via silver filled epoxy, H-417 (Table 1).

Figures 21, 22, and 23 are the plots of the H215-2 circuit. The raw data (Figure 21) and the normalized and averaged data (Figure 22) are of the thermal impedance of junction to case. The normalized and averaged data of thermal impedance of the junction to static ambient air (Figure 23) are also presented. This circuit (-2) was an epoxy mounted die, multilayer substrate with the substrate to header bond via silver filled epoxy H-417 (Table 1).

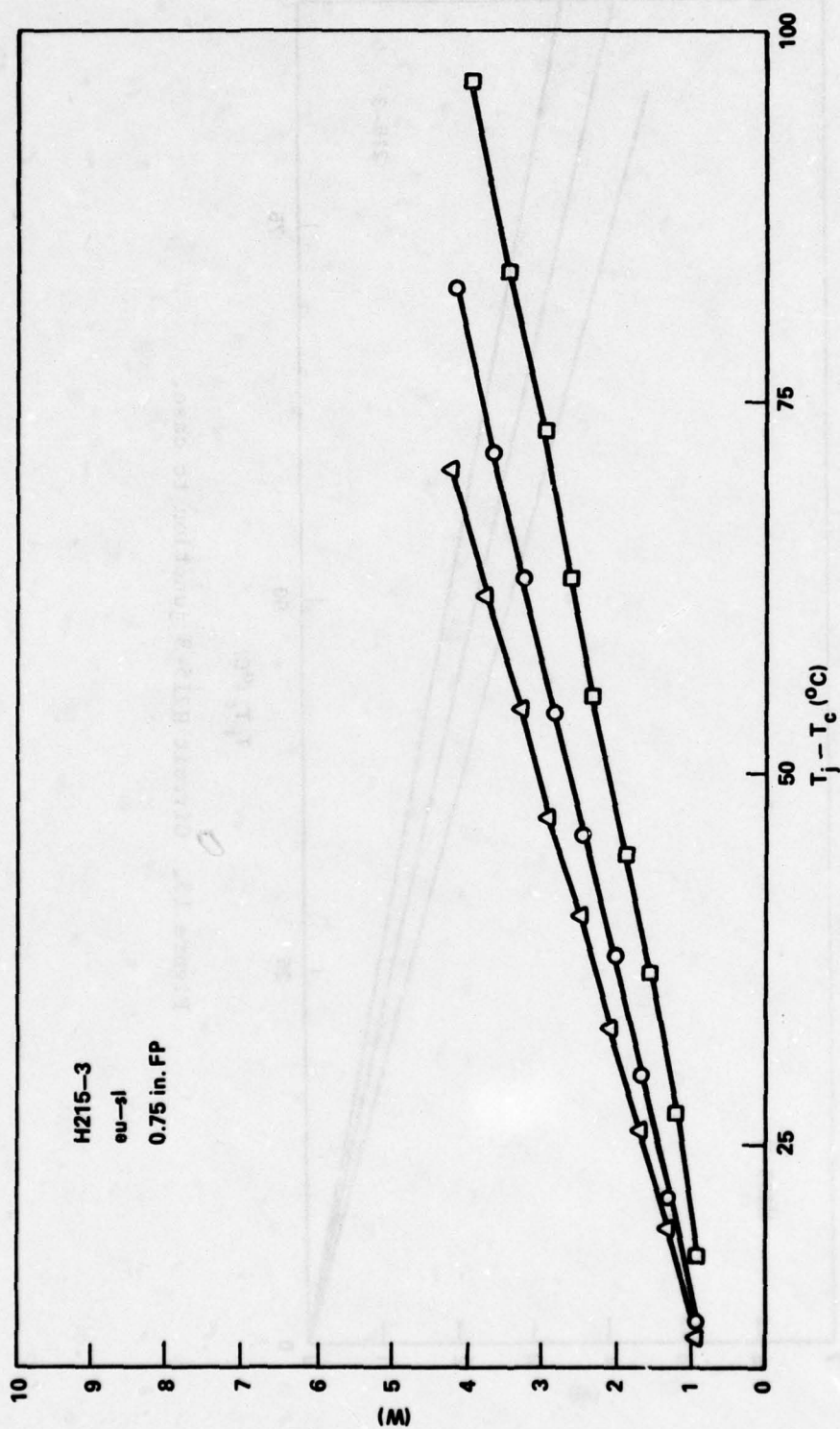


Figure 12. Circuit H215-3 raw data.



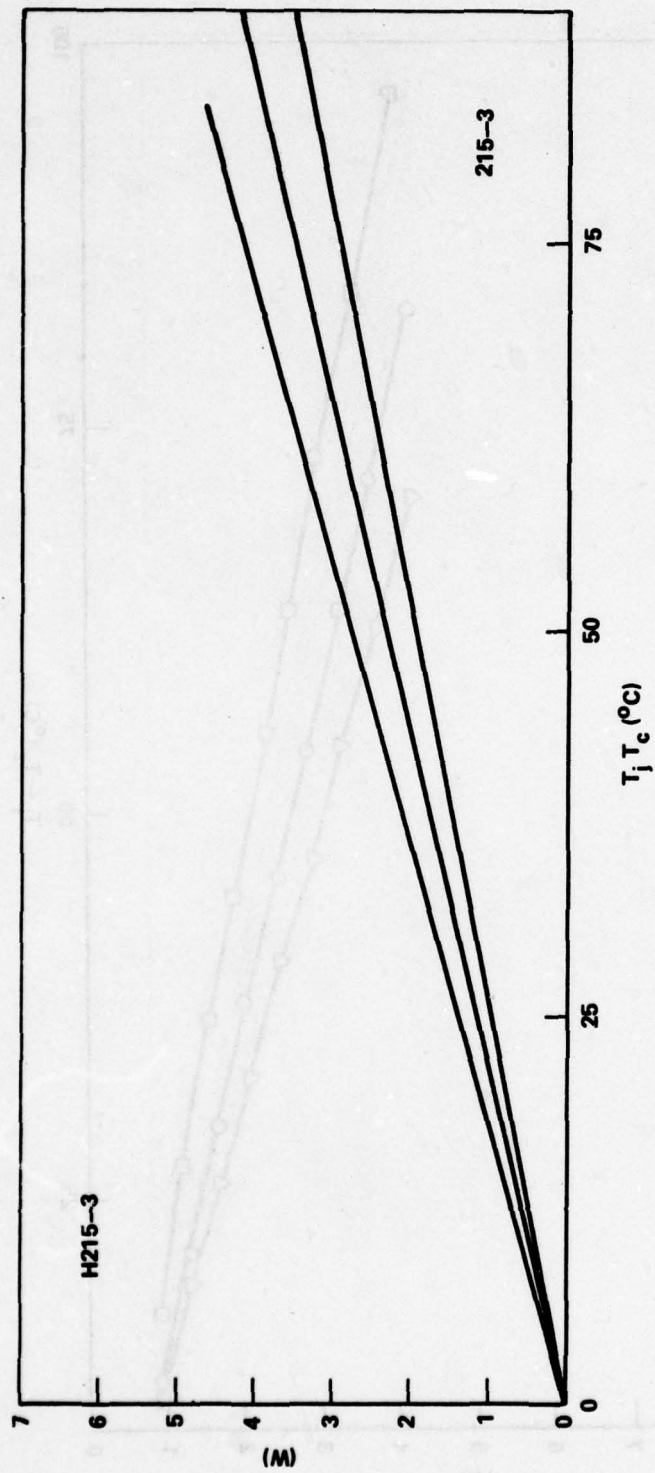


Figure 13. Circuit H215-3 junction to case.

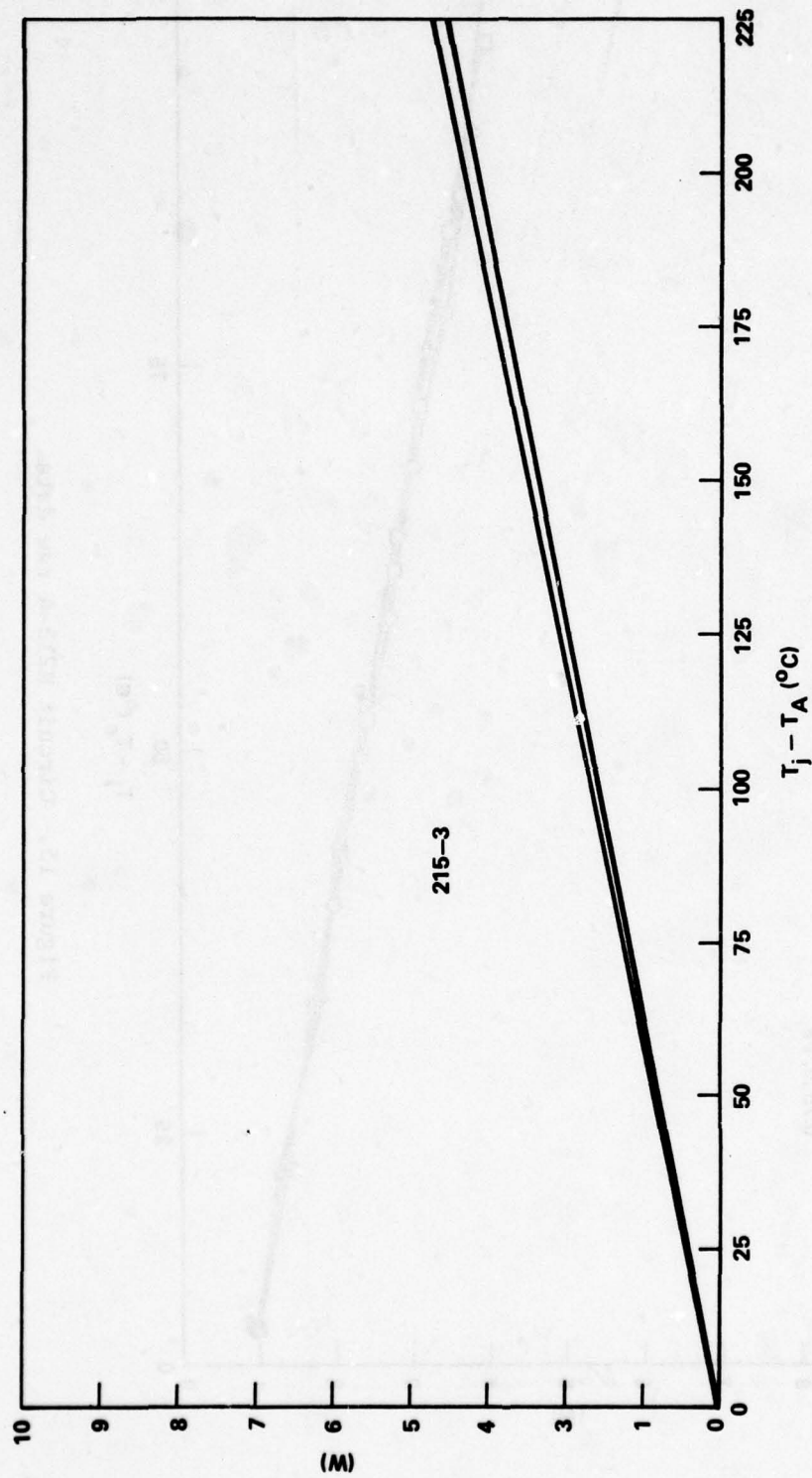


Figure 14. Circuit H215-3 junction to ambient.

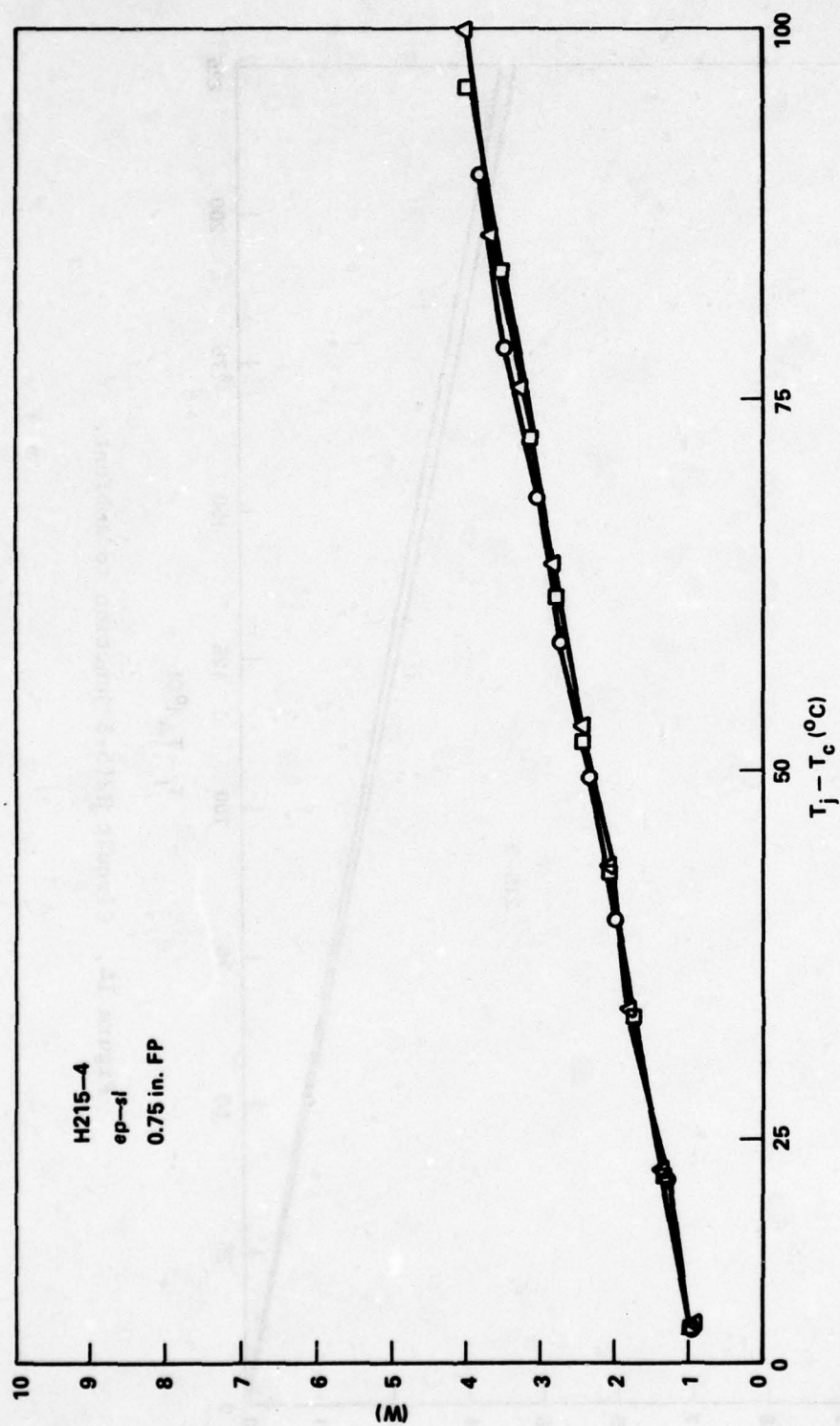


Figure 15. Circuit H215-4 raw data.



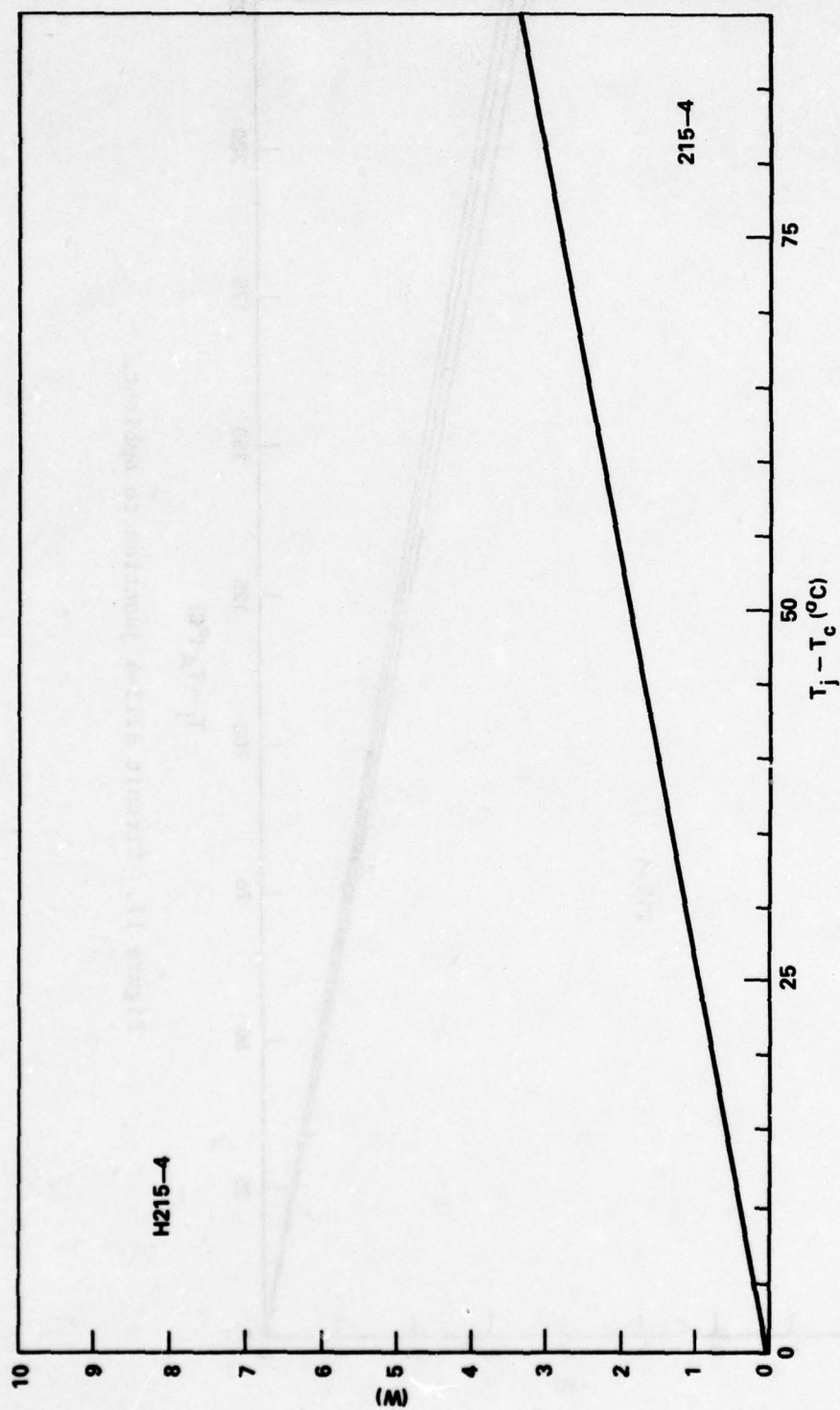


Figure 16. Circuit H215-4 junction case.

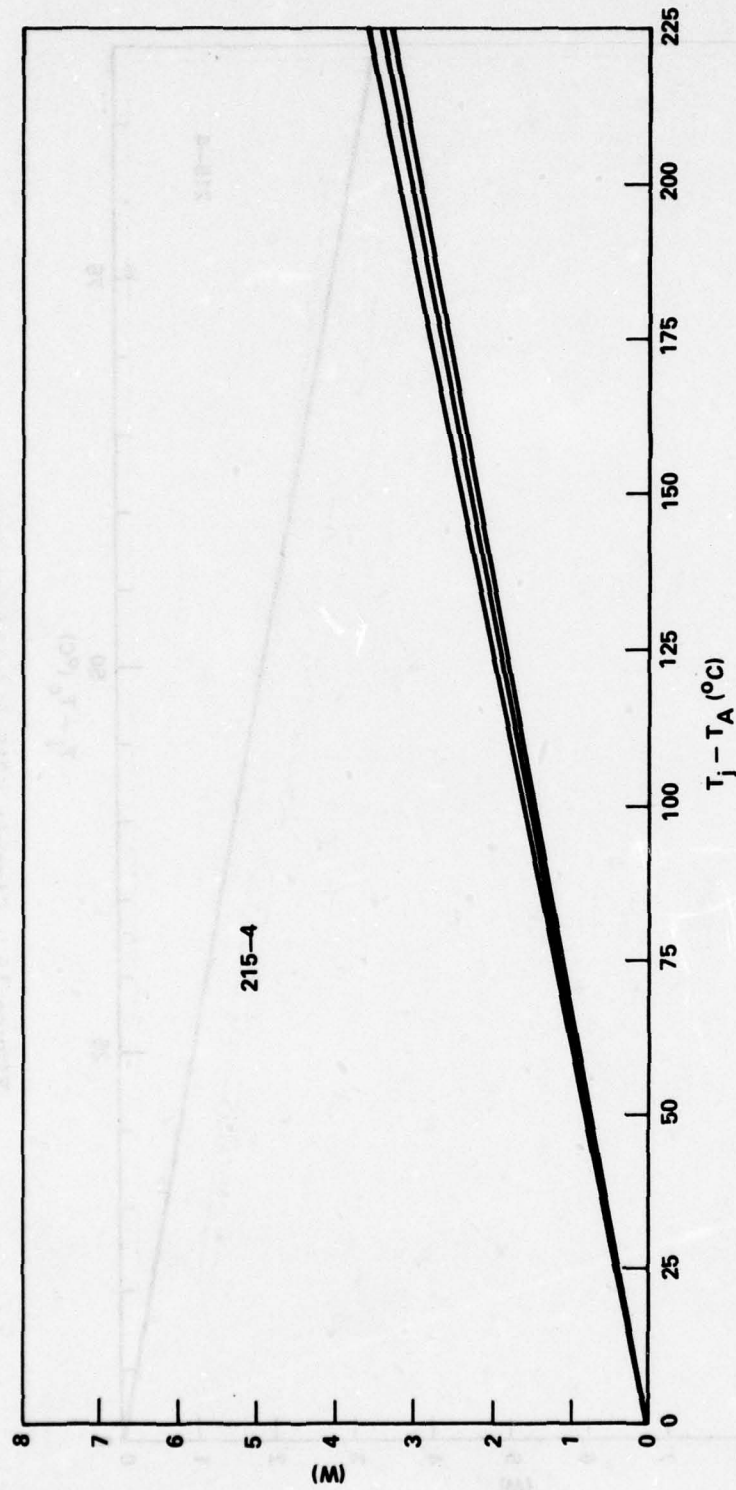


Figure 17. Circuit H215-4 junction to ambient.

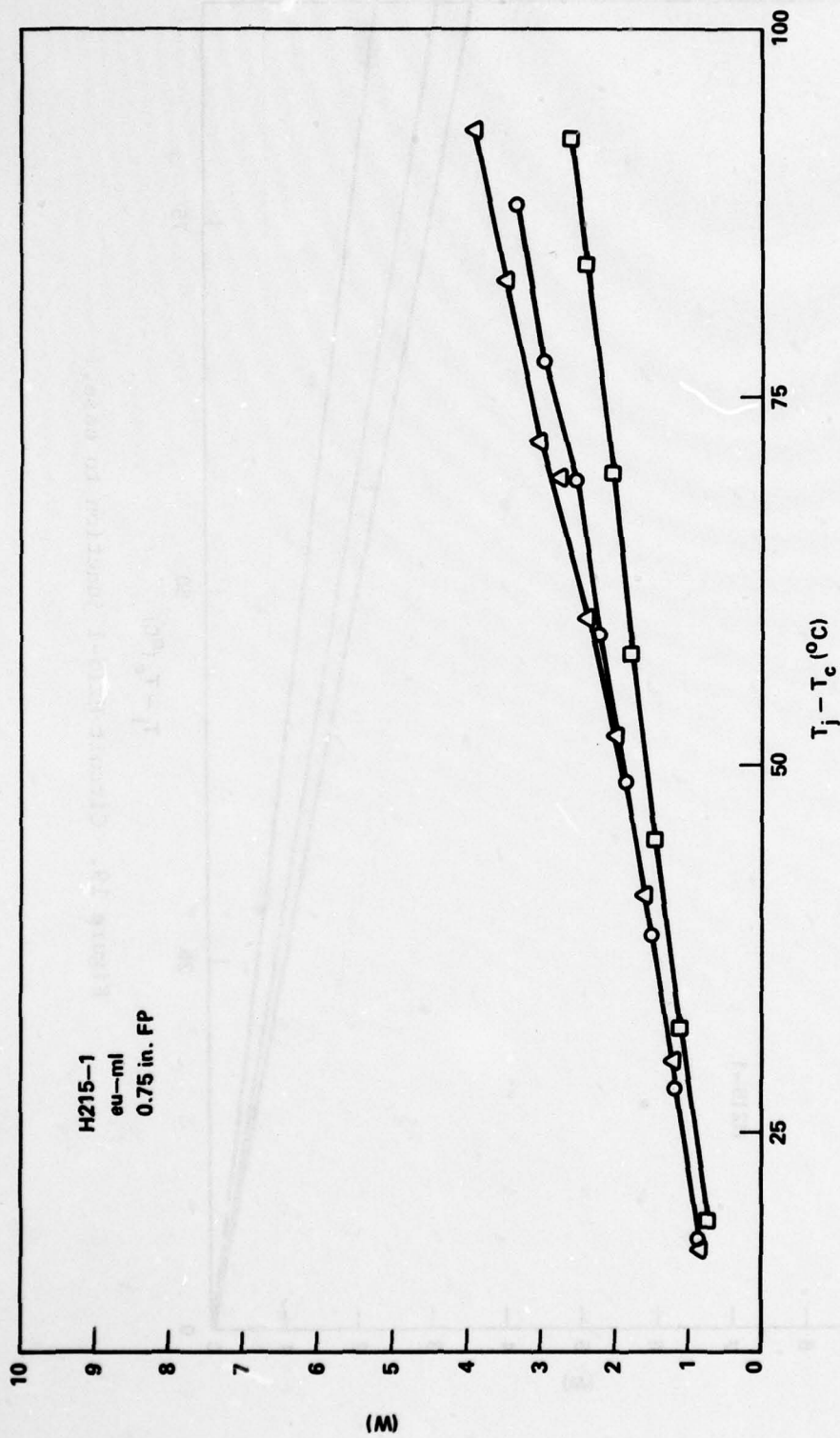


Figure 18. Circuit H215-1 raw data.



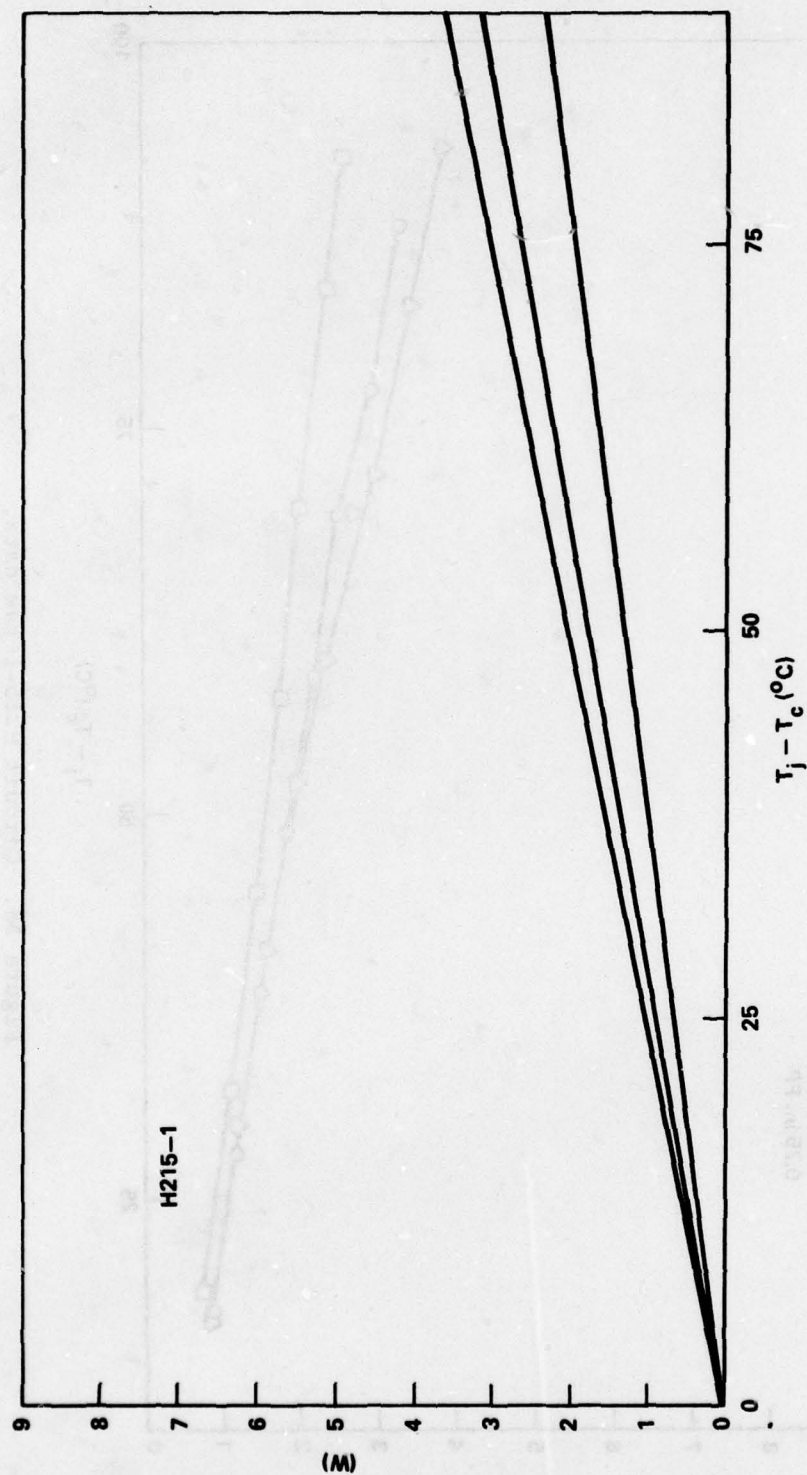


Figure 19. Circuit H215-1 junction to case.

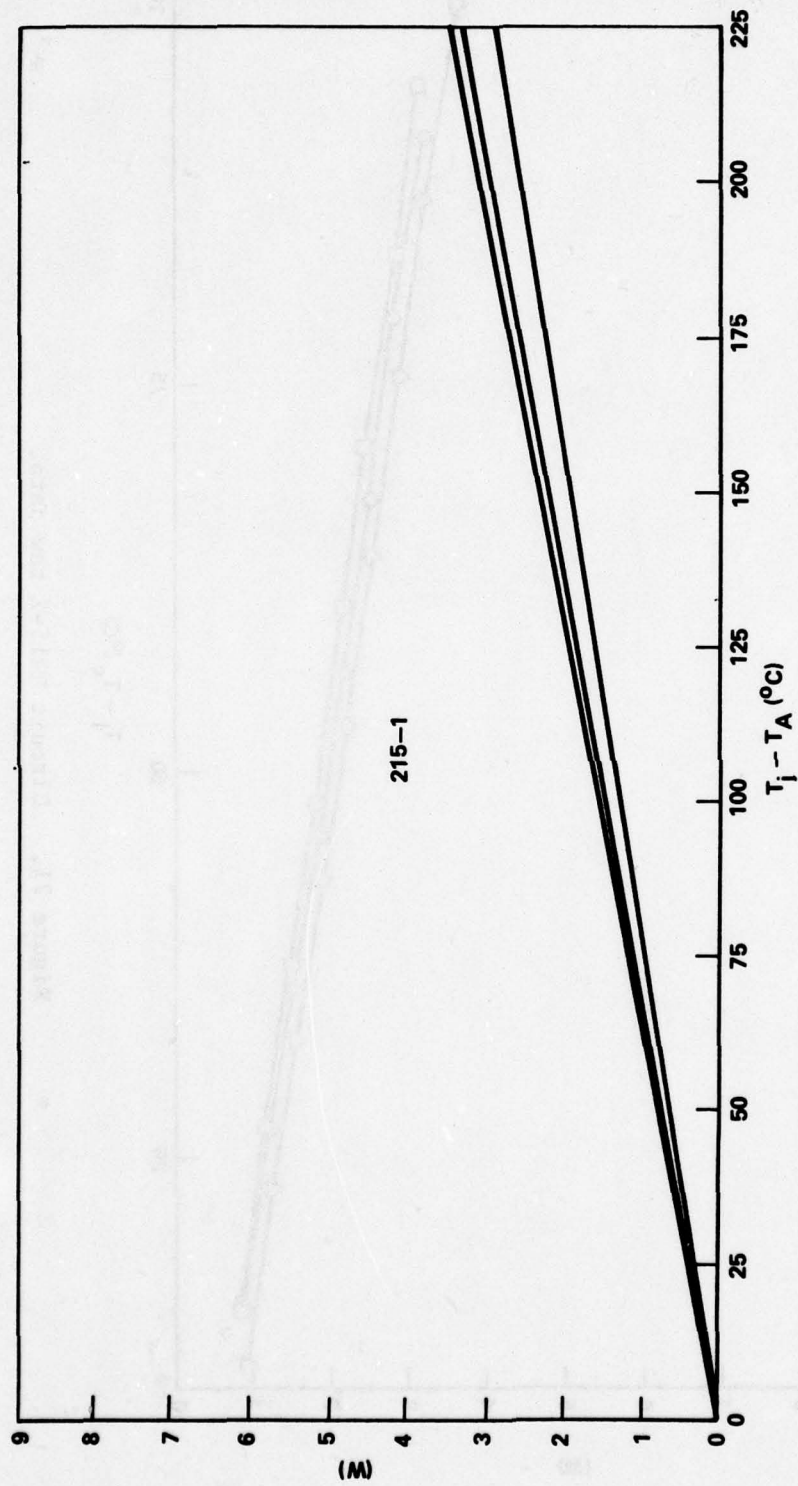


Figure 20. Circuit H215-1 junction to ambient.

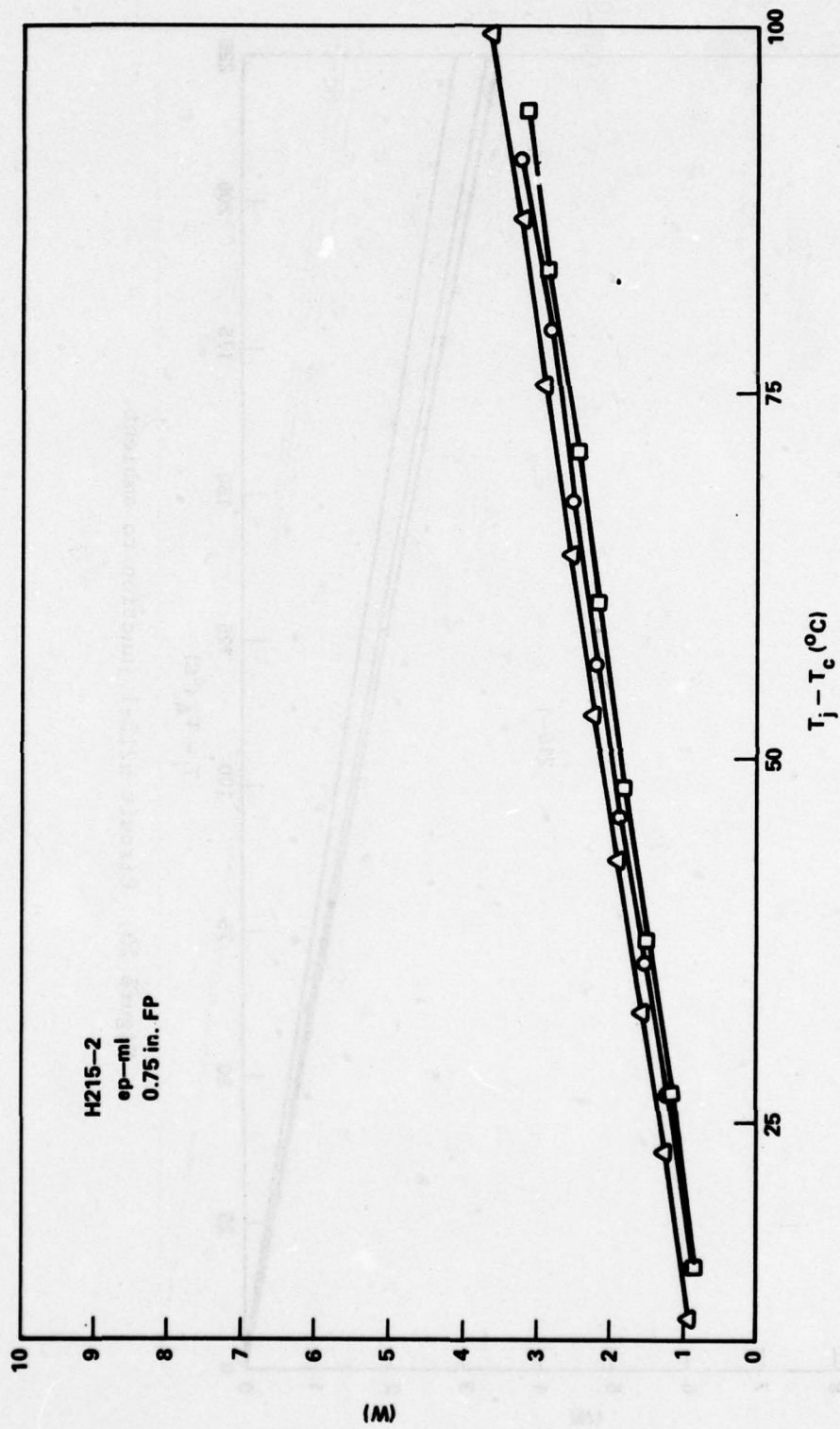


Figure 21. Circuit H215-2 raw data.



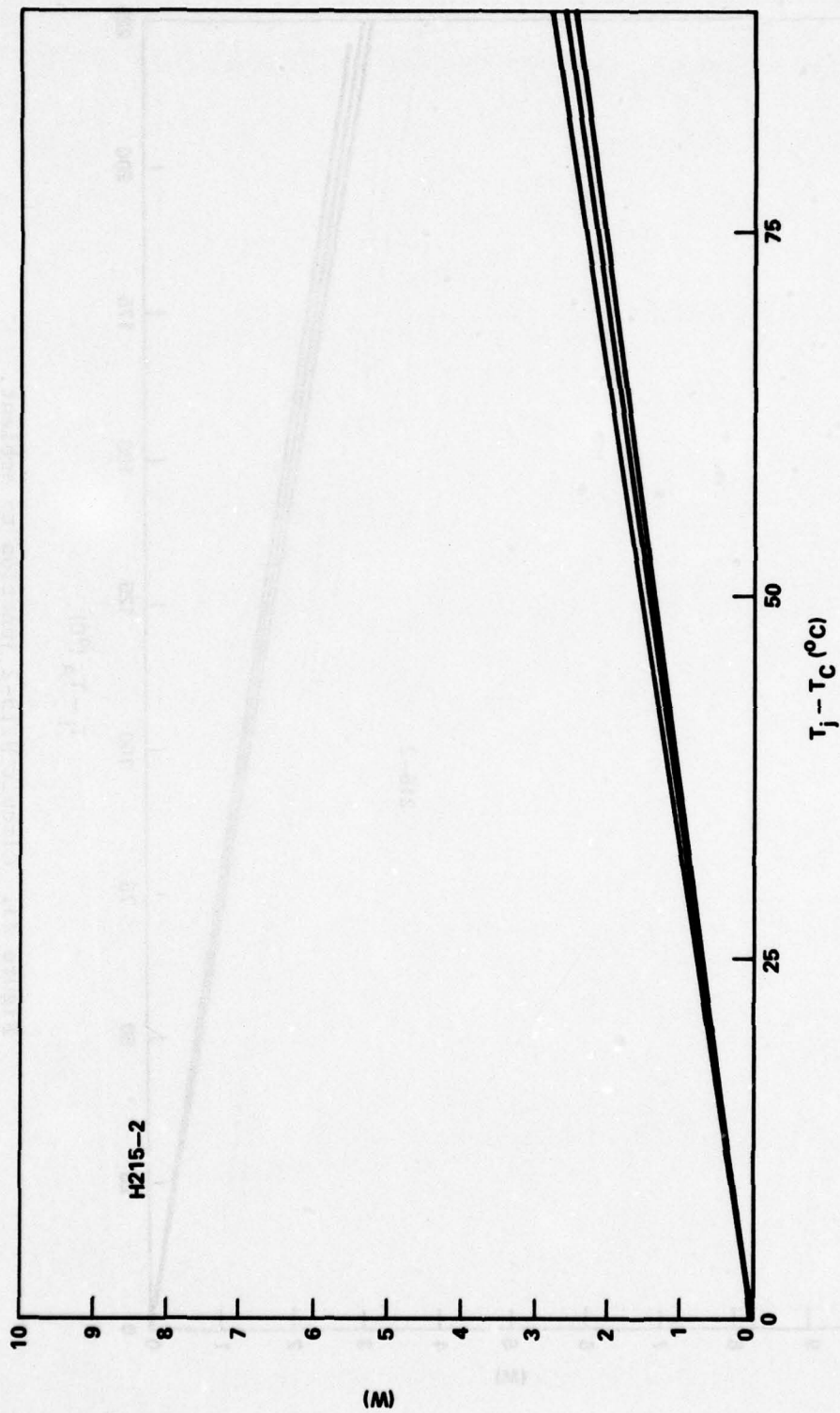


Figure 22. Circuit H215-2 junction to case.

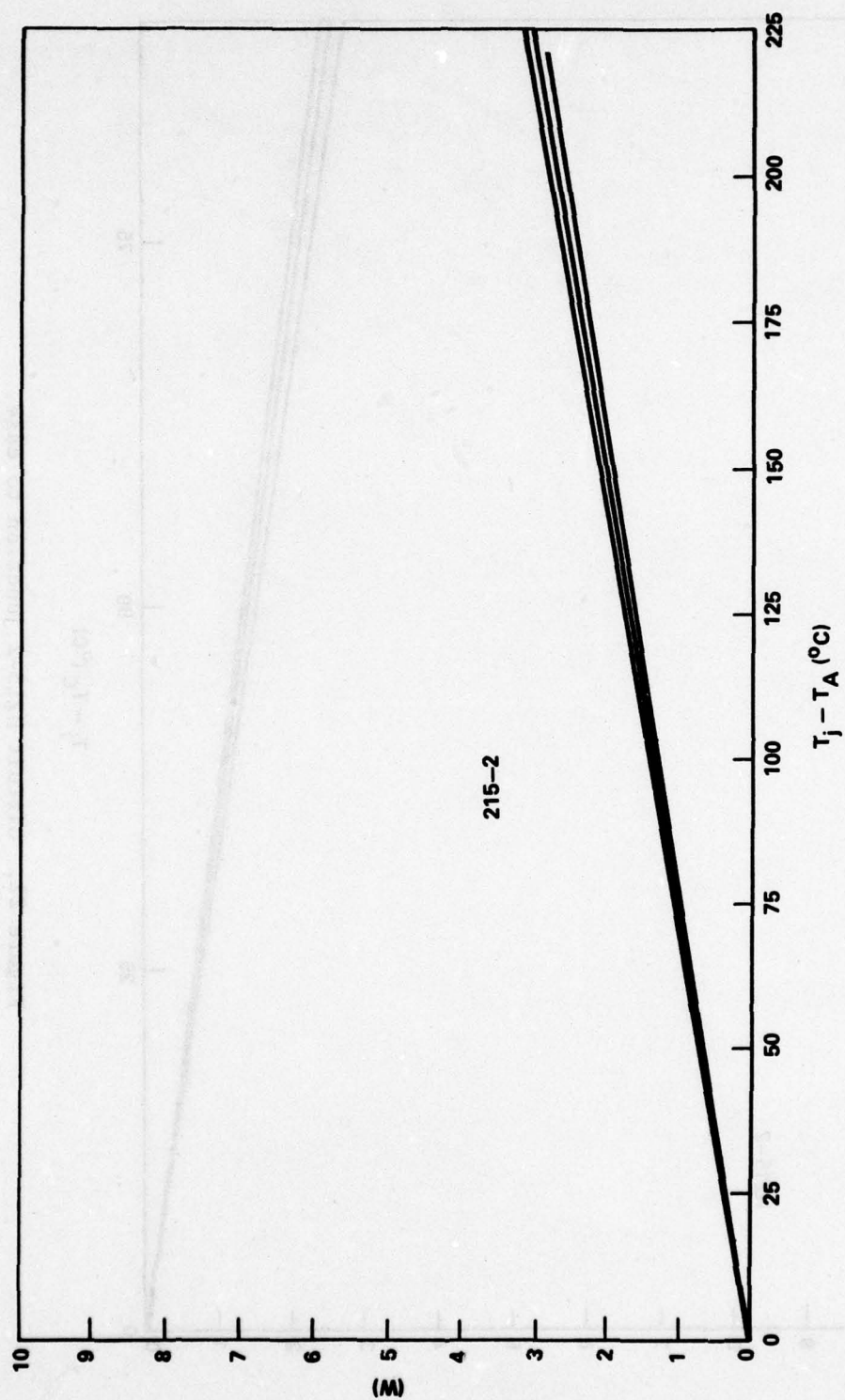


Figure 23. Circuit H215-2 junction to ambient.

## 2. Thermal Characteristics of a 1-in. Flat Pack

The thermal impedance data for a 1-in. flat pack designated as circuit H214 are given in Figures 24 to 35. Figures 24, 25, and 26 are plots of the H214-3 circuit for the raw data (Figure 24), the normalized and averaged data (Figure 25) and the thermal impedance of junction to static ambient air  $\theta_{ja}$  (Figure 26). This circuit (-3) was a eutectically mounted die single layer substrate and substrate to header bond with H-417.

Figures 27, 28, and 29 are plots of the H214-4 circuit. Figure 27 presents the raw data. Figure 28 is the  $\theta_{jc}$  (linearized and normalized). Figure 29 is the  $\theta_{jc}$ . This circuit (-4) was epoxy die mounted (H-41), single layer substrate, and substrate to header bond with silver filled epoxy (H-417).

Figures 30, 31, and 32 are the plots of the H214-1 circuit. The raw data (Figure 30) and the normalized and averaged data (Figure 31) are of the thermal impedance of junction to case. The normalized and averaged data of the thermal impedance of the junction to static ambient air (Figure 32) are also presented. This circuit (-1) was a eutectically mounted die, multilayer substrate with the substrate to header bond via silver filled epoxy (H417).

Figures 33, 34, and 35 are the plots of the H214-2 circuit. The raw data (Figure 33) and the normalized and averaged data (Figure 34) are of the thermal impedance of junction to case. The normalized and averaged data of thermal impedance of the junction to static ambient air (Figure 35) are also presented. This circuit (-2) is with the substrate to header bond of silver filled epoxy (H-417).



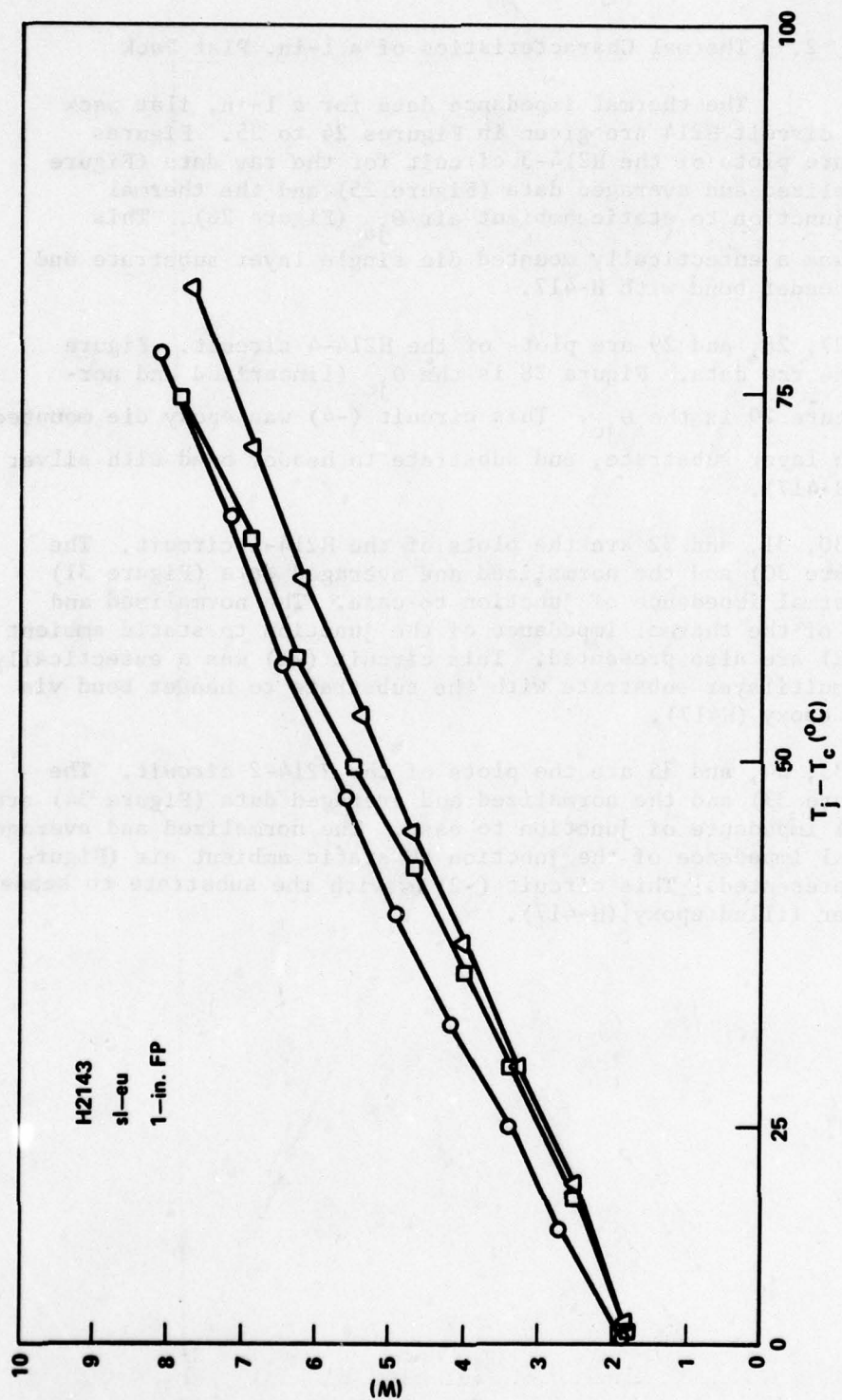


Figure 24. Circuit H214-3 raw data.

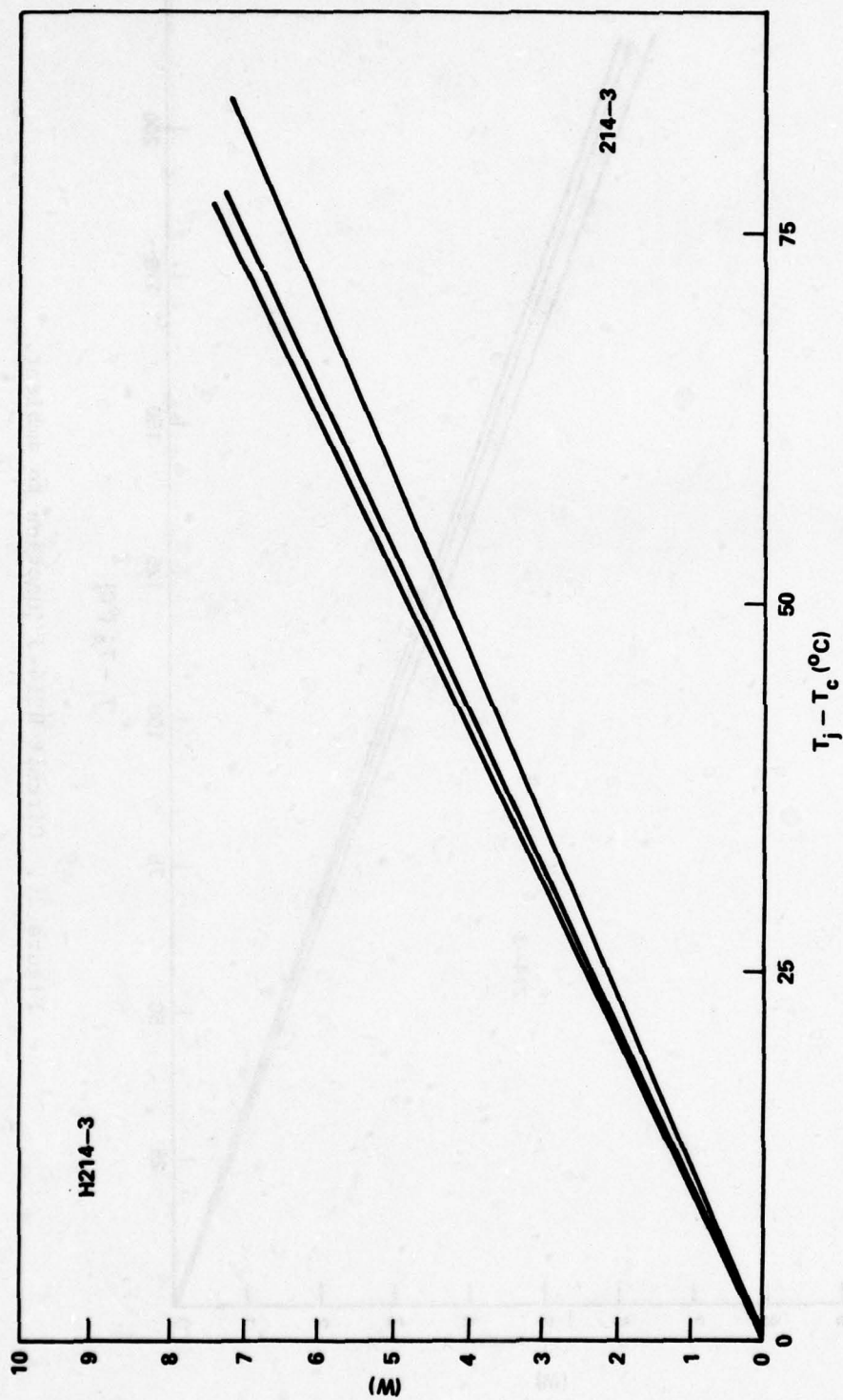


Figure 25. Circuit H214-3 junction case.

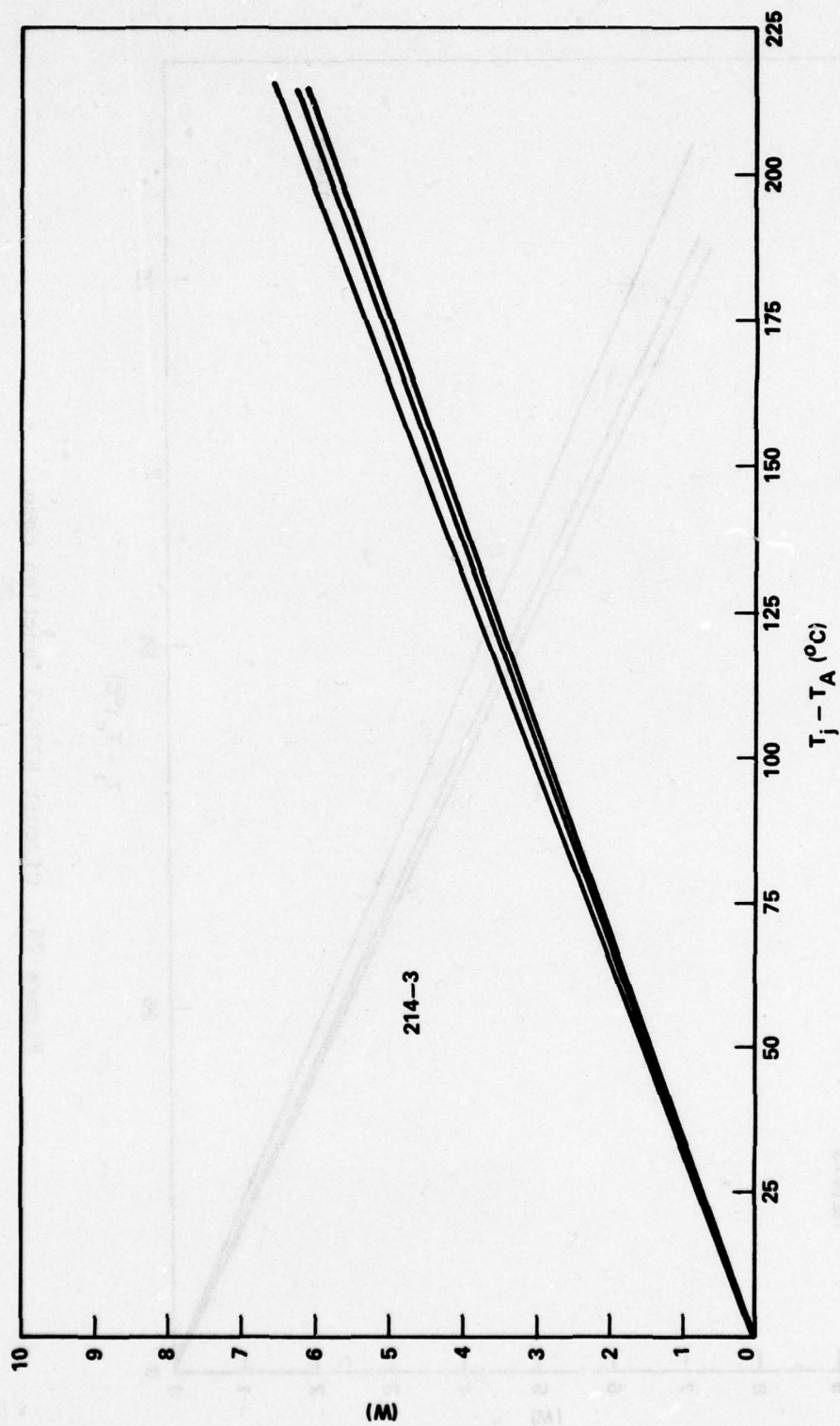


Figure 26. Circuit H214-3 junction to ambient.



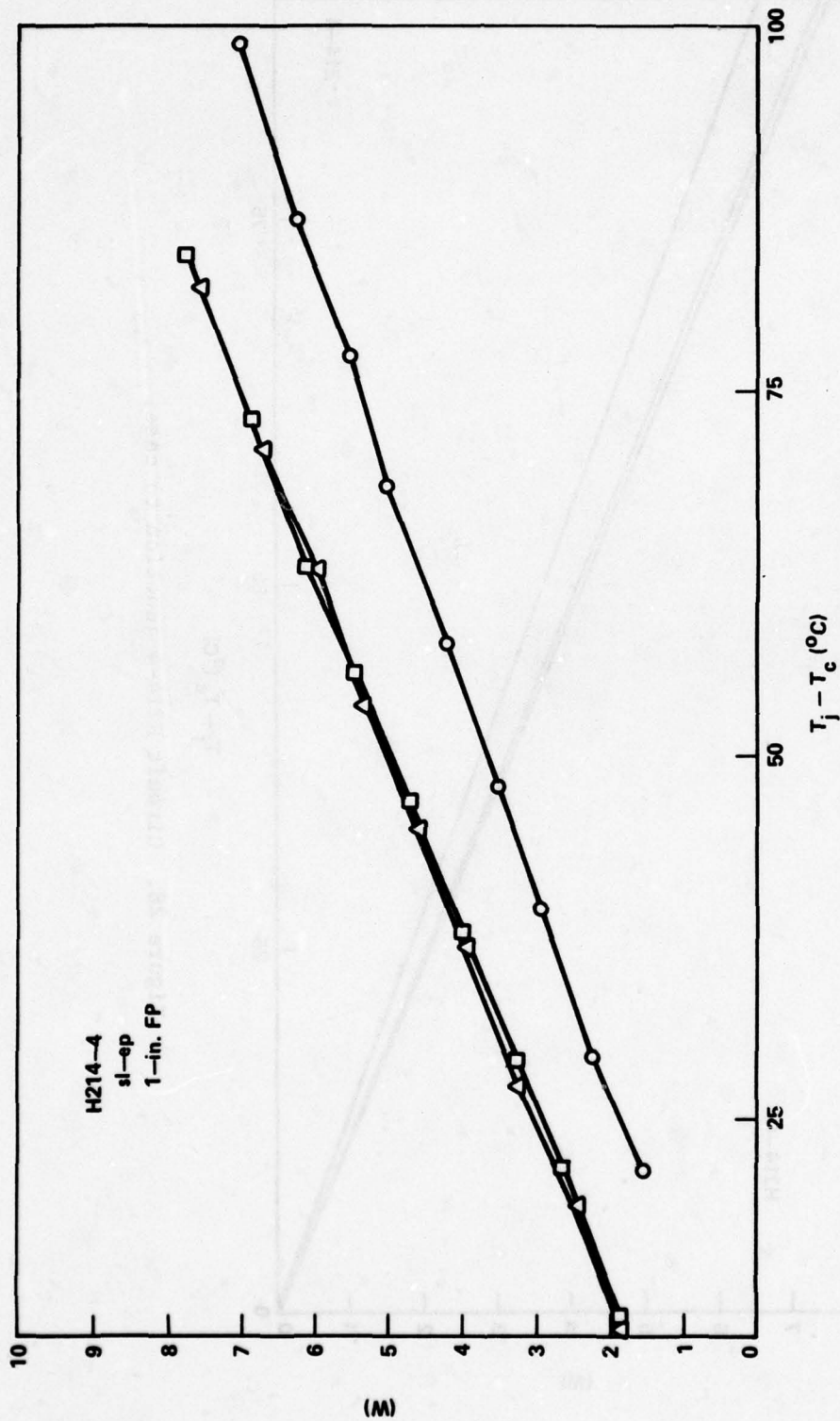


Figure 27. Circuit H214-4 raw data.

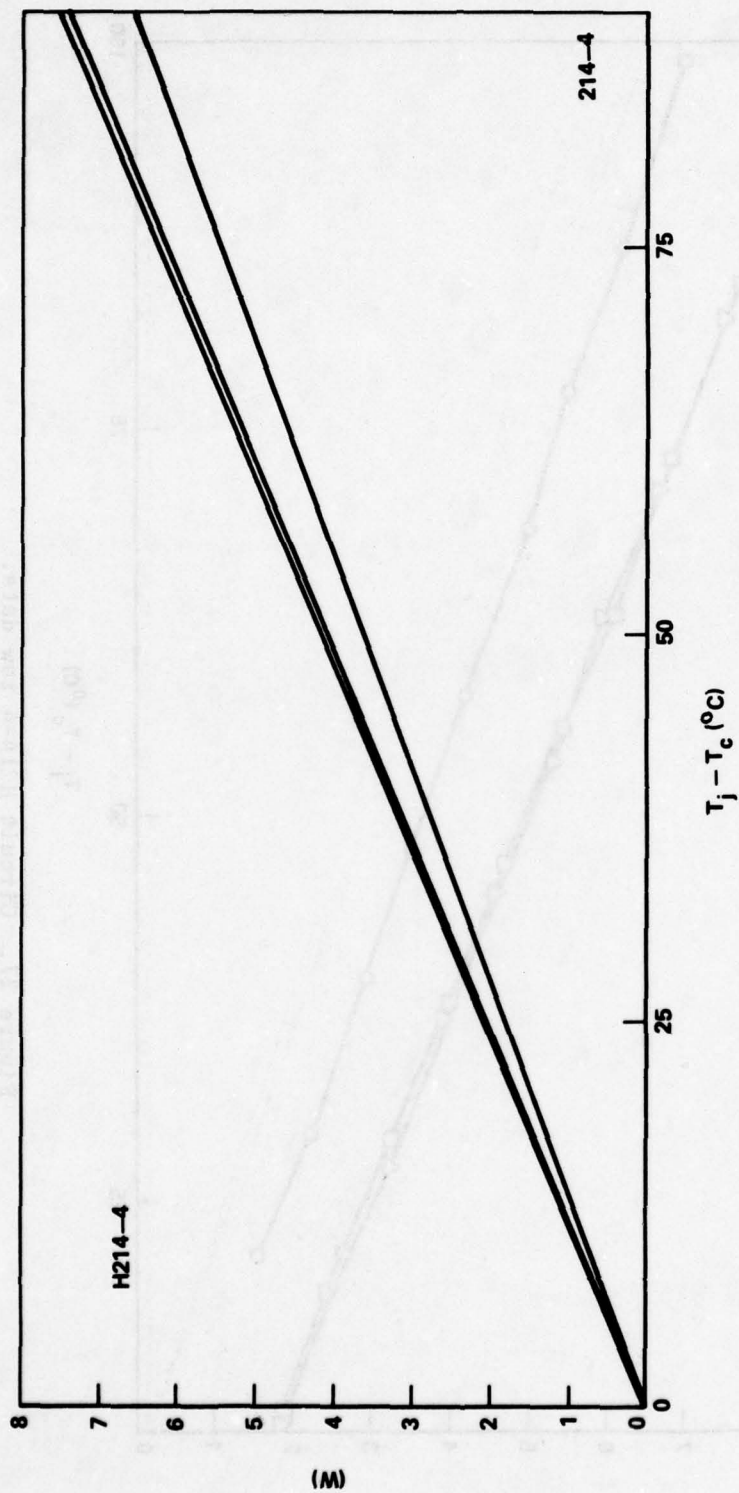


Figure 28. Circuit H214-4 junction to case.

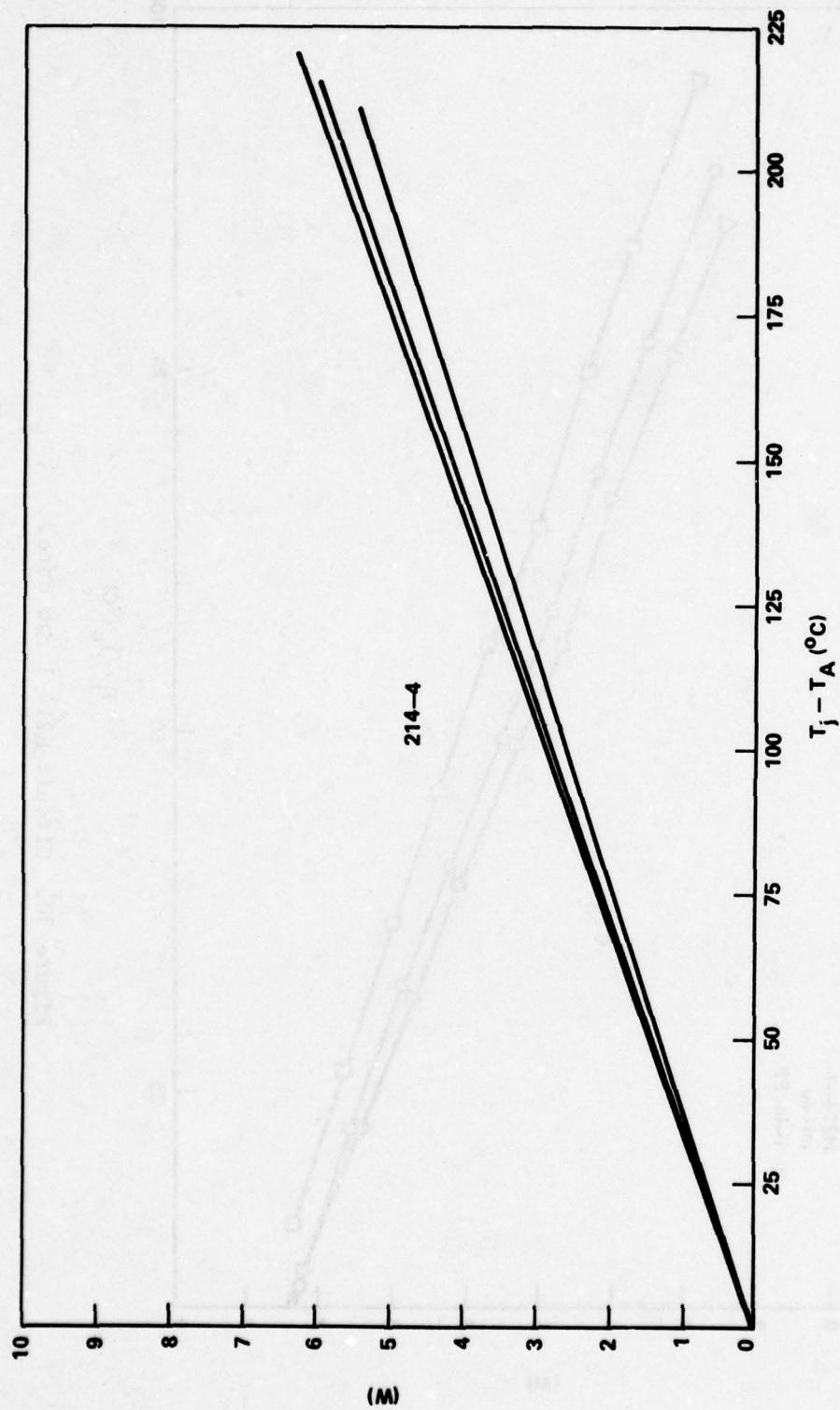


Figure 29. Circuit H214-4 junction to ambient.



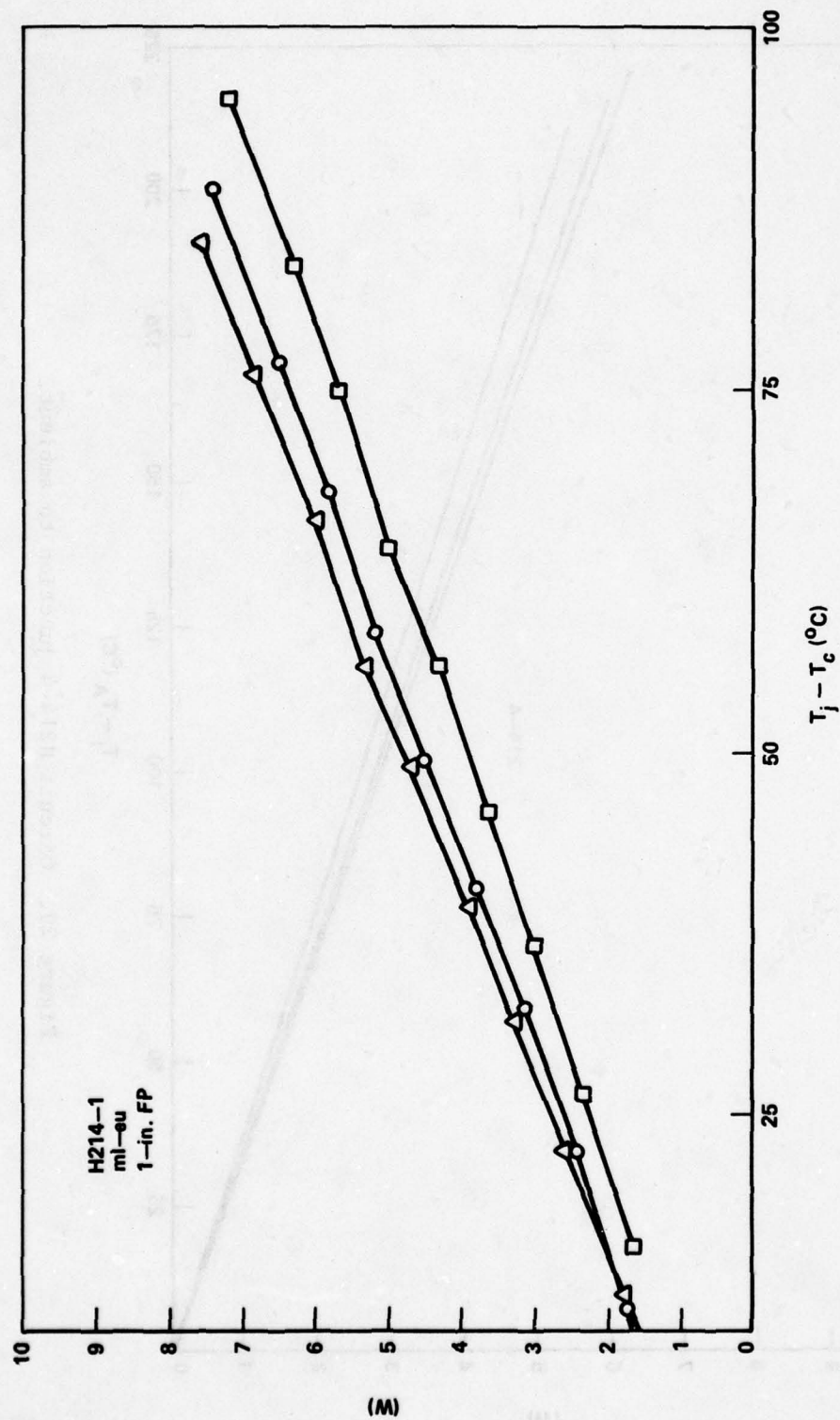


Figure 30. Circuit H214-1 raw data.

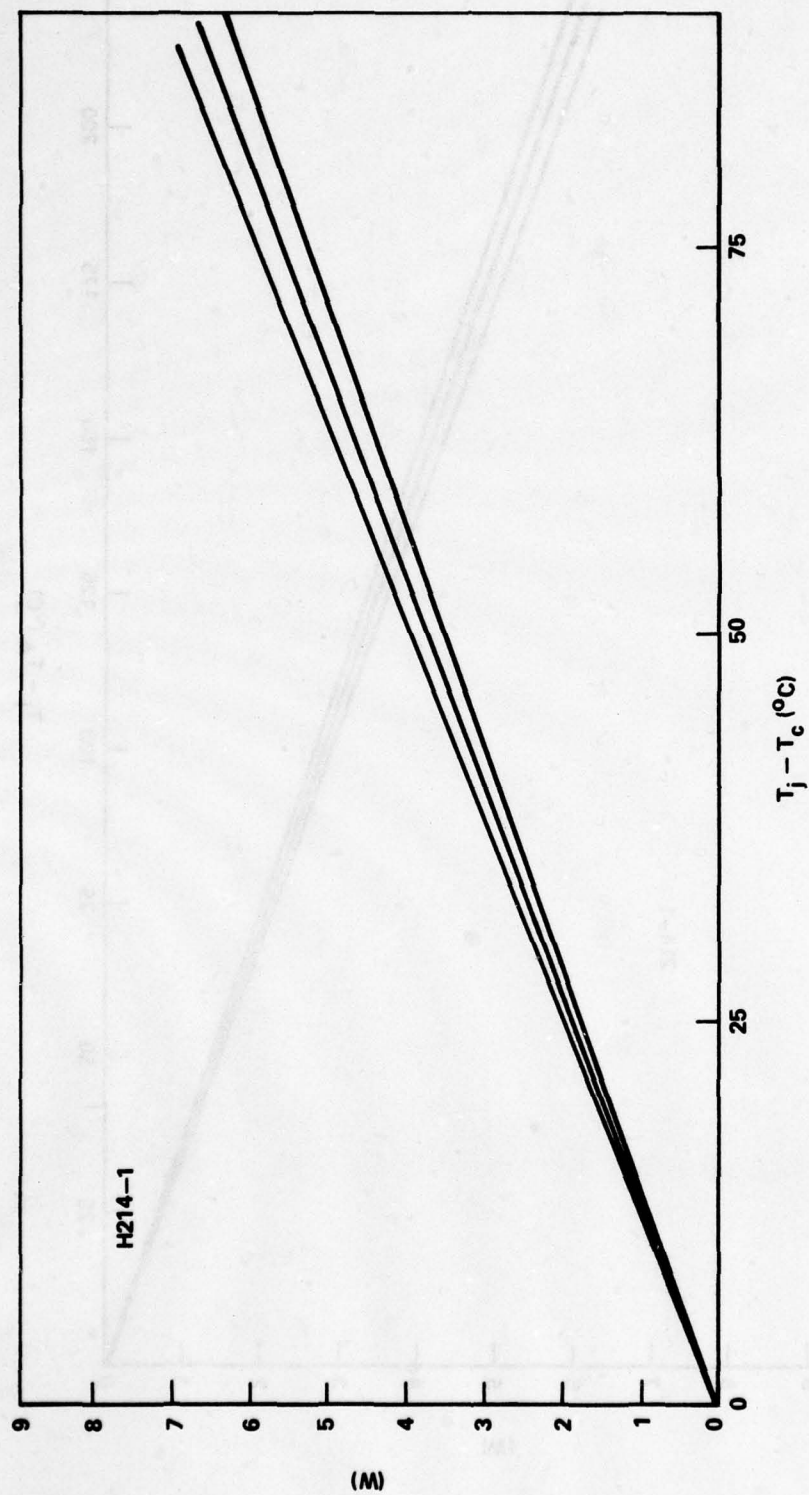


Figure 31. Circuit H214-1 junction to case.

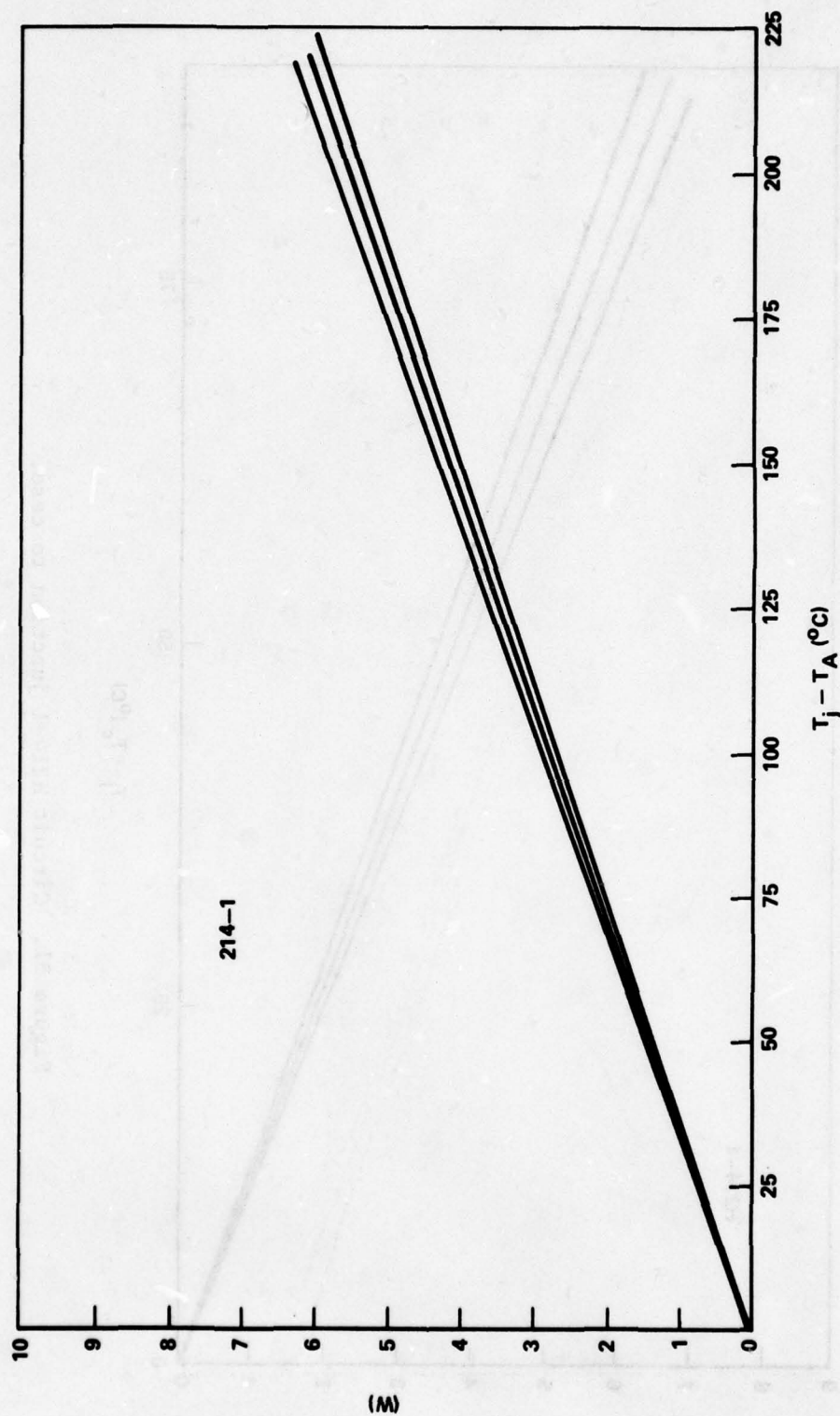


Figure 32. Circuit H214-4 junction to ambient.



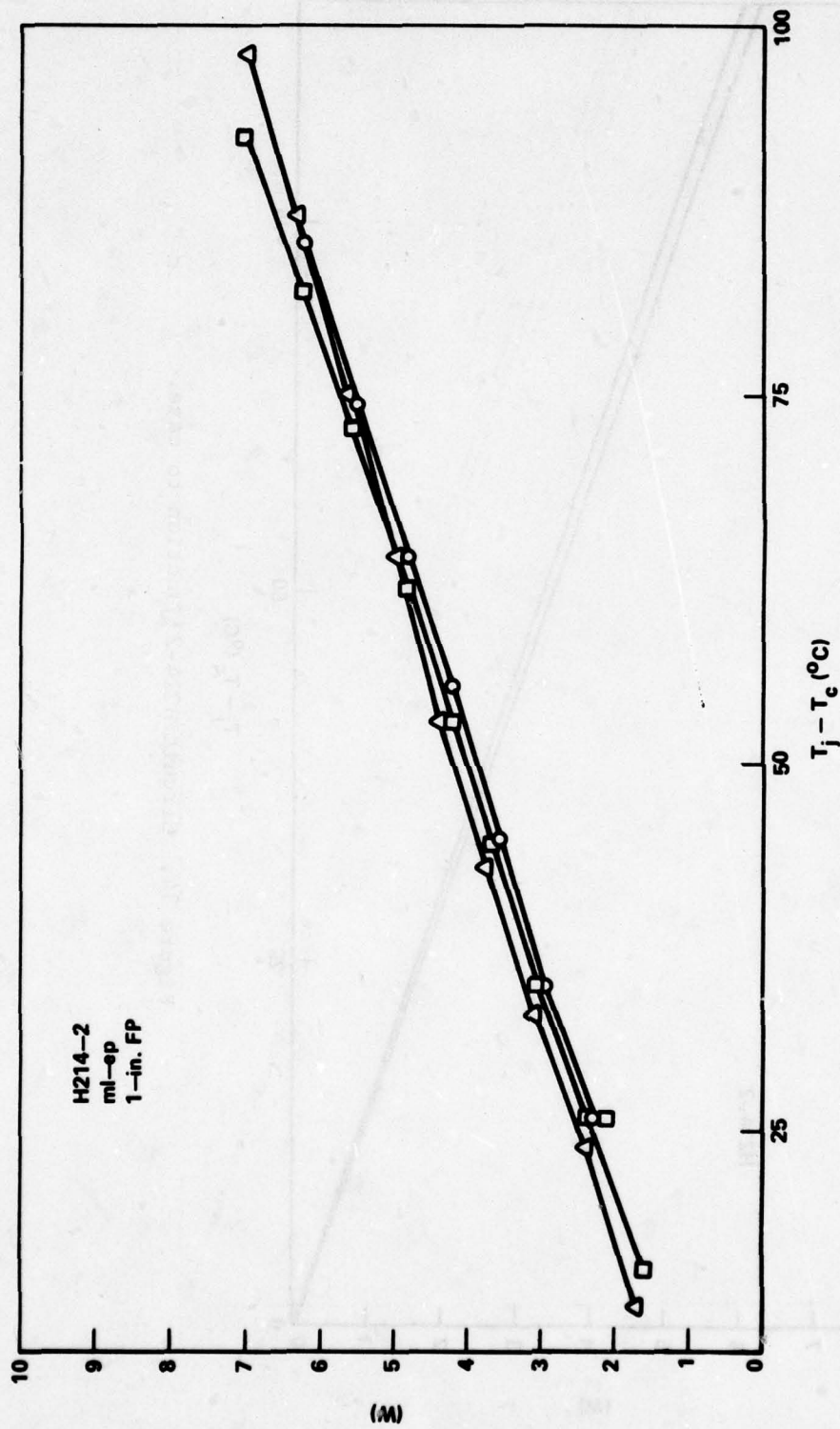


Figure 33. Circuit H214-2 raw data.

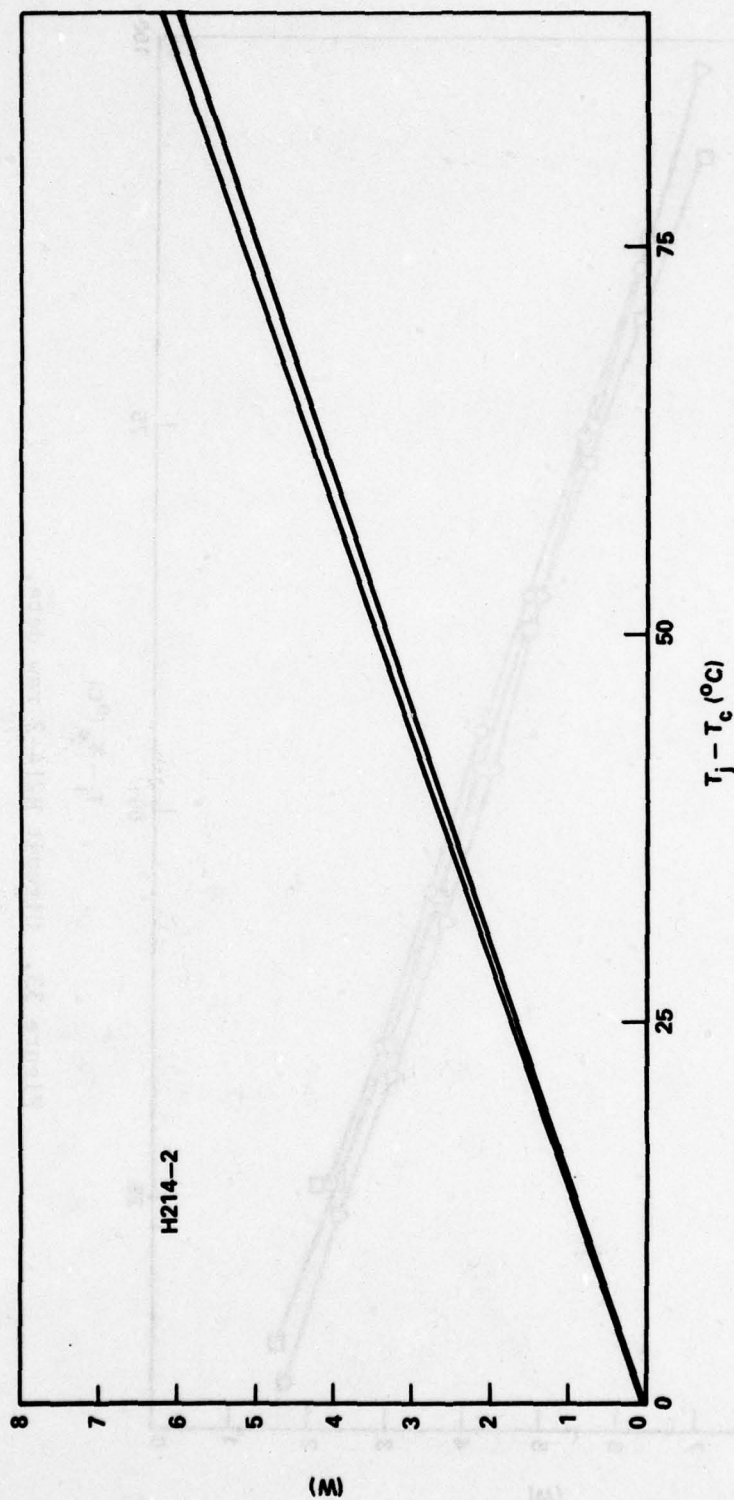


Figure 34. Circuit H214-2 junction to case.

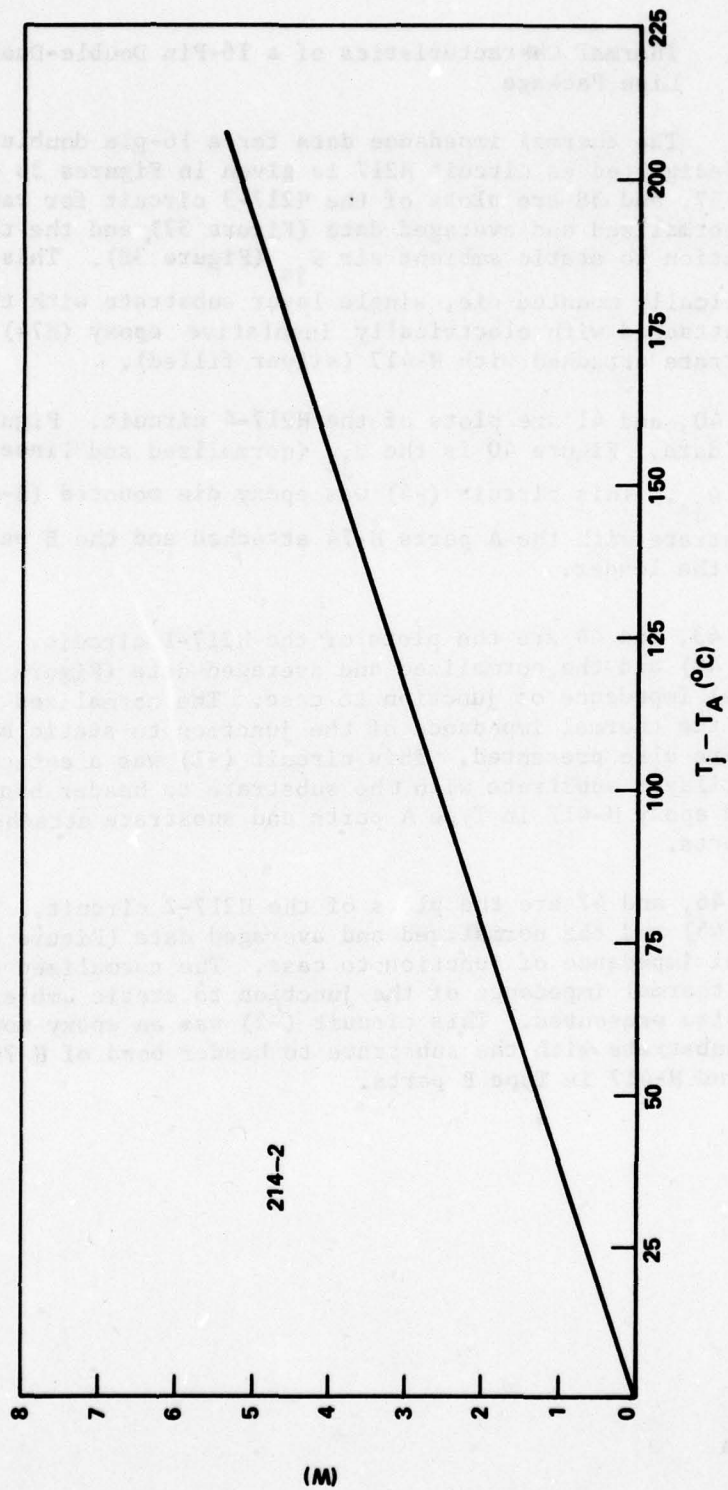


Figure 35. Circuit H214-2 junction to ambient.



### 3. Thermal Characteristics of a 16-Pin Double-Dual-In-Line Package

The thermal impedance data for a 16-pin double-dual in-line package designated as circuit H217 is given in Figures 36 through 47. Figures 36, 37, and 38 are plots of the H217-3 circuit for raw data (Figure 36), the normalized and averaged data (Figure 37), and the thermal impedance of junction to static ambient air  $\theta_{ja}$  (Figure 38). This circuit (-3) was a eutectically mounted die, single layer substrate with the A parts substrate attached with electrically insulative epoxy (H74) and the B parts substrate attached with H-417 (silver filled).

Figures 39, 40, and 41 are plots of the H217-4 circuit. Figure 39 presents the raw data. Figure 40 is the  $\theta_{jc}$  (normalized and linearized). Figure 41 is the  $\theta_{ja}$ . This circuit (-4) was epoxy die mounted (H-41), single layer substrate with the A parts H-74 attached and the B parts H-417 attached to the leader.

Figures 42, 43, and 44 are the plots of the H217-1 circuit. The raw data (Figure 42) and the normalized and averaged data (Figure 43) are of the thermal impedance of junction to case. The normalized and averaged data of the thermal impedance of the junction to static ambient air (Figure 44) are also presented. This circuit (-1) was a eutectically mounted die, multilayer substrate with the substrate to header bond via silver filled epoxy H-417 in Type A parts and substrate attached with H-74 in Type B parts.

Figures 45, 46, and 47 are the plots of the H217-2 circuit. The raw data (Figure 45) and the normalized and averaged data (Figure 46) are of the thermal impedance of junction to case. The normalized and averaged data of thermal impedance of the junction to static ambient air (Figure 47) are also presented. This circuit (-2) was an epoxy mounted die, multilayer substrate with the substrate to header bond of H-74 in Type A parts and H-417 in Type B parts.

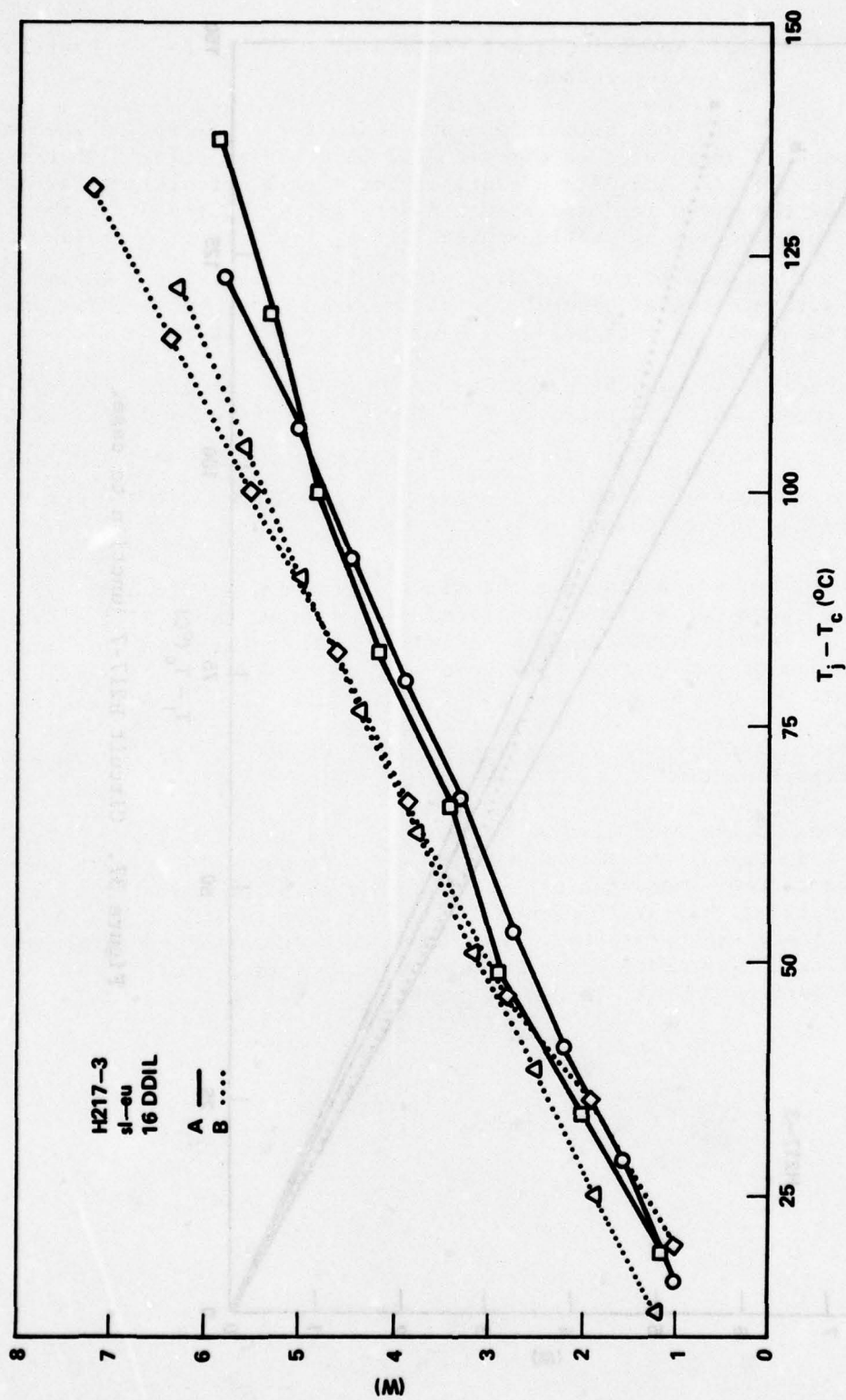


Figure 36. Circuit H217-3 raw data.

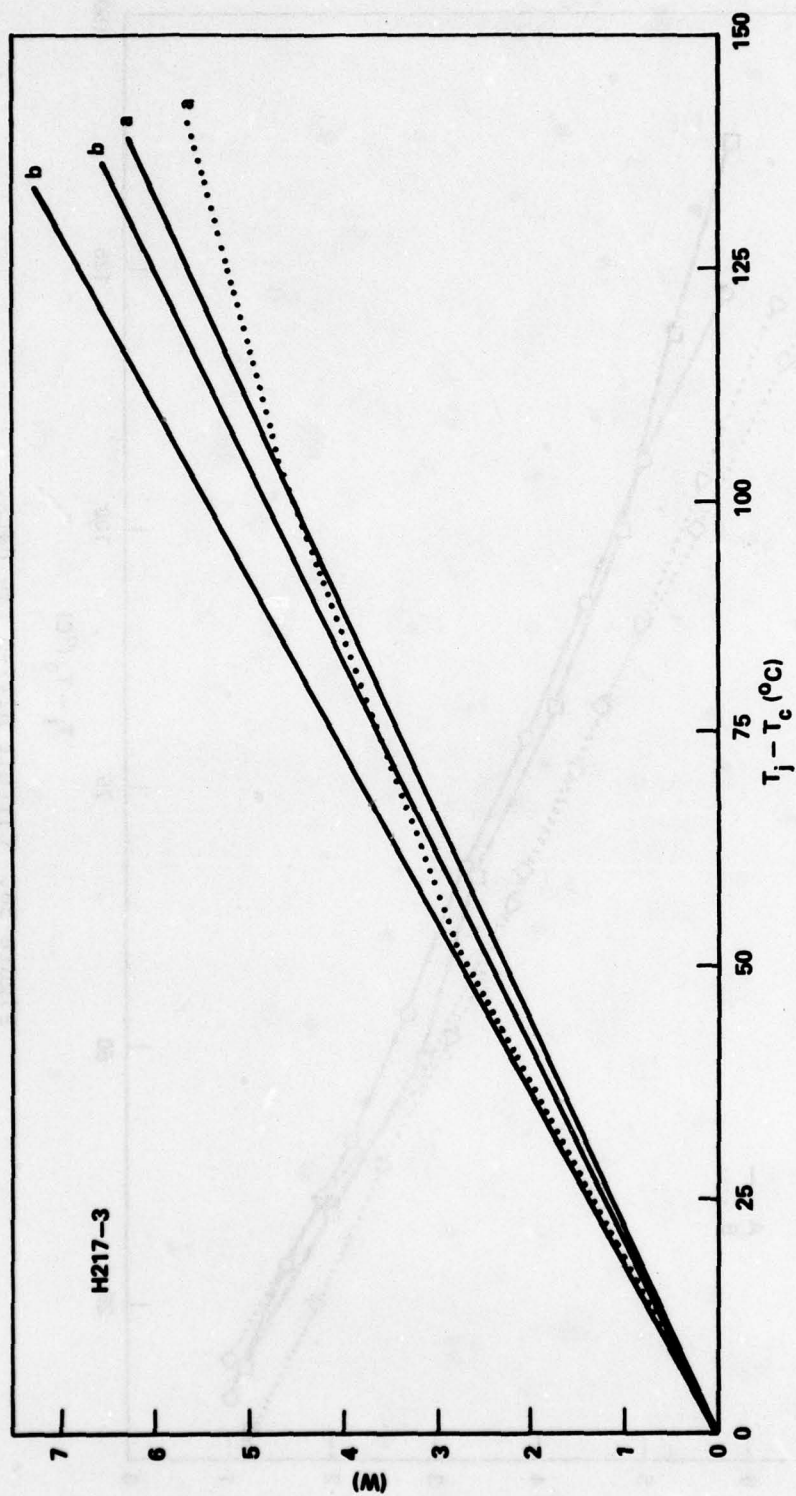


Figure 37. Circuit H217-7 junction to case.



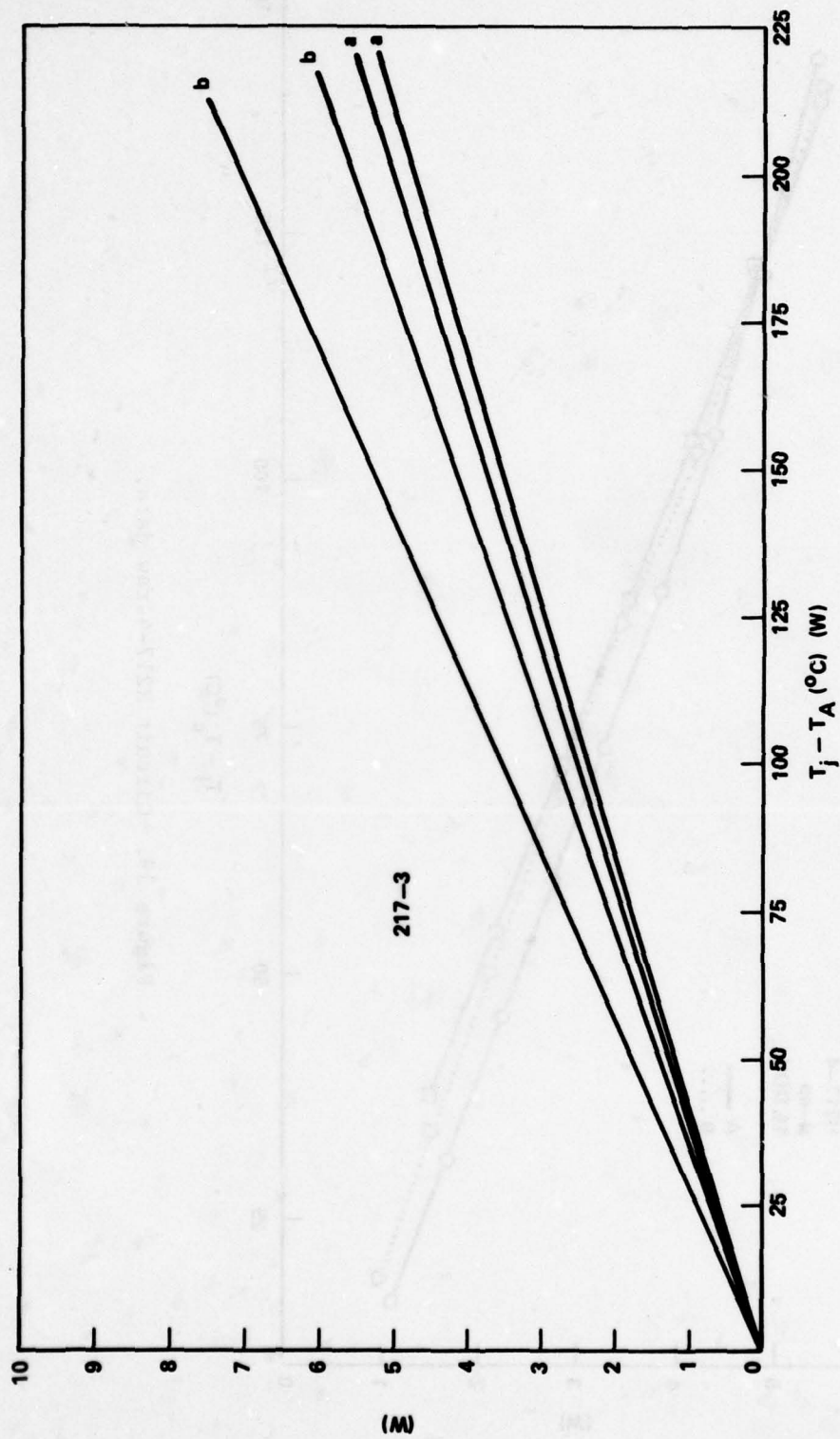


Figure 38. Circuit H217-3 junction to ambient.

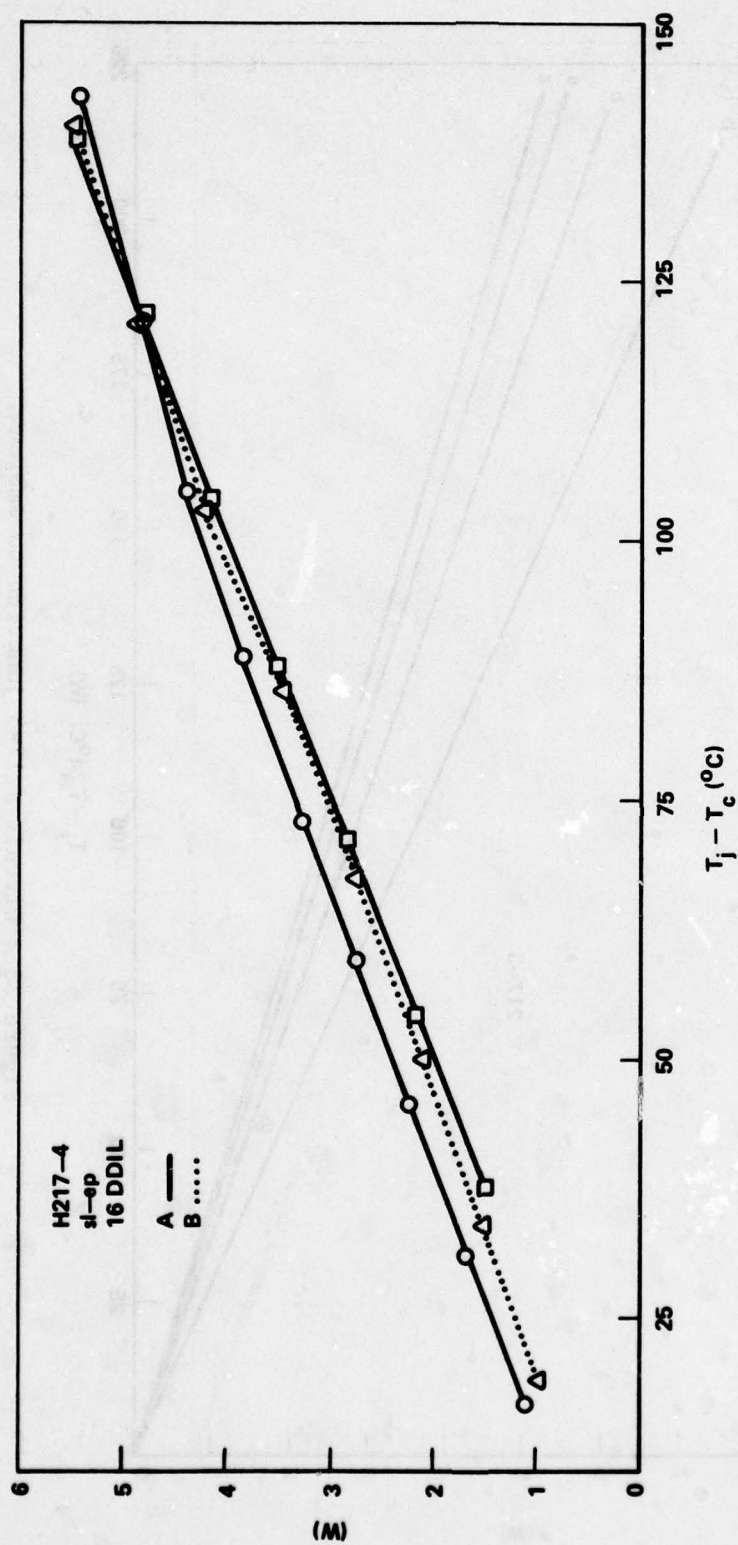


Figure 39. Circuit H217-4 raw data.



Figure 40. Circuit H217-4 junction to case.



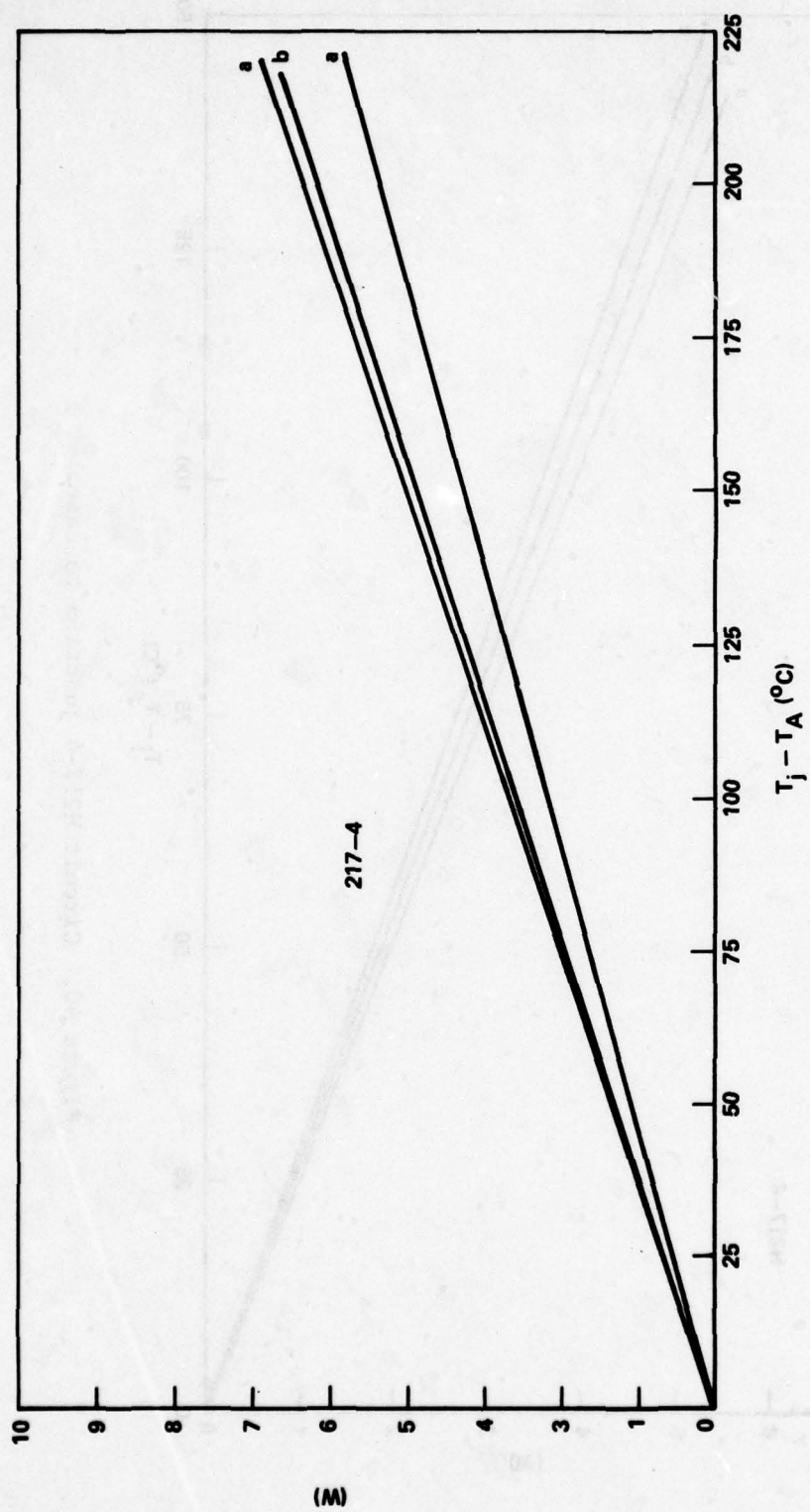


Figure 41. Circuit H217-4 junction to ambient.

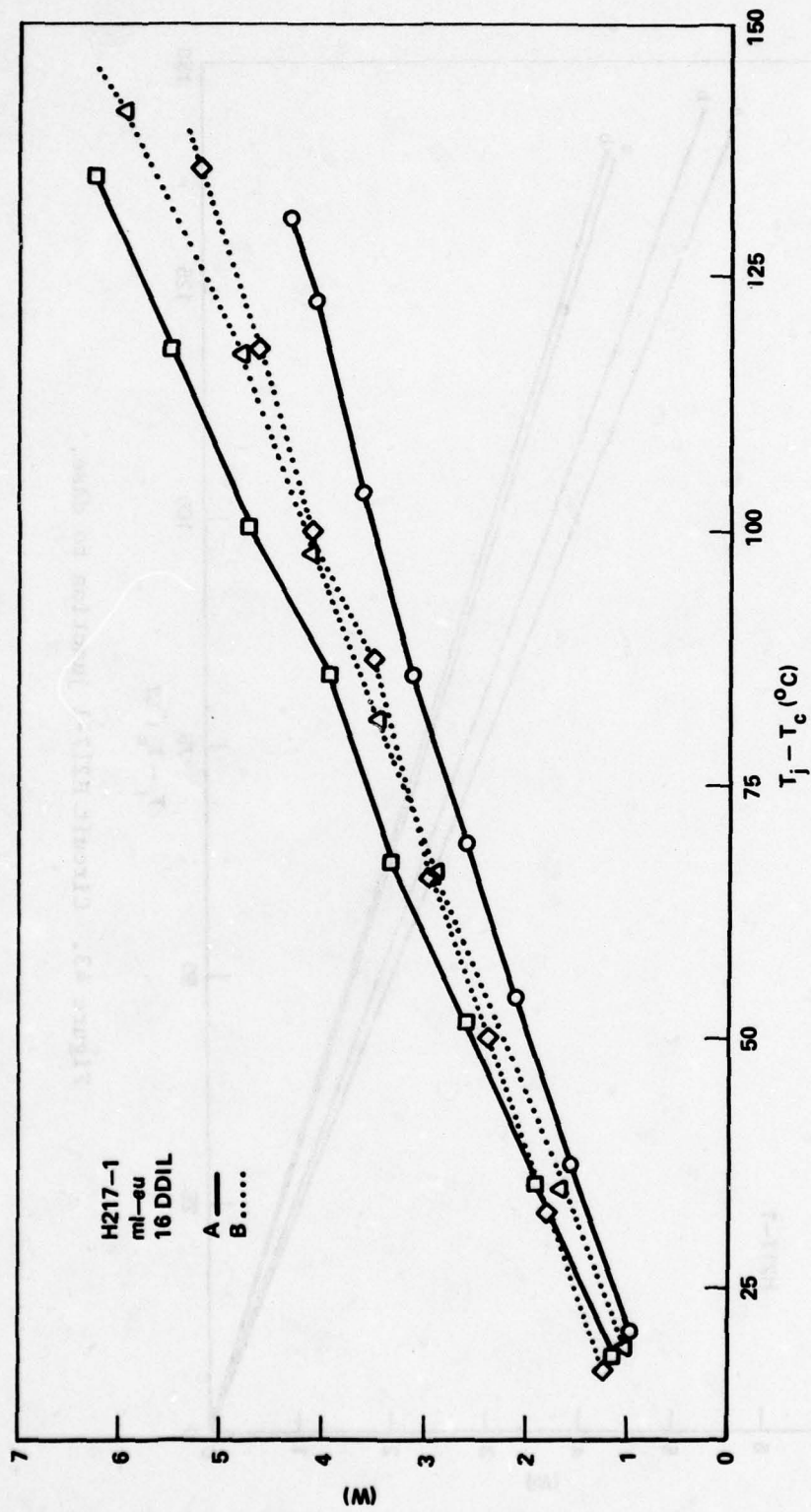


Figure 42. Circuit H217-1 raw data.

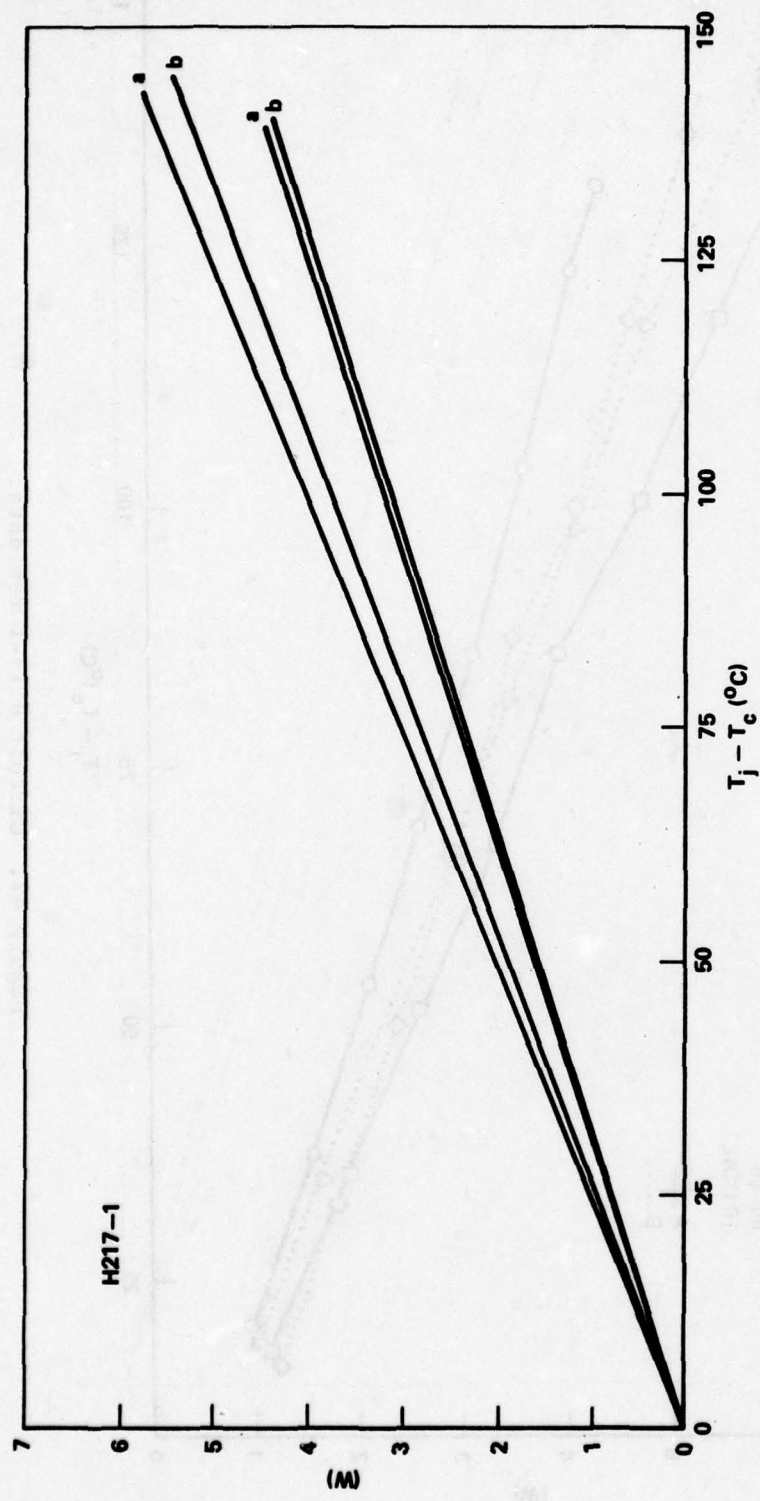


Figure 43. Circuit H217-1 junction to case.



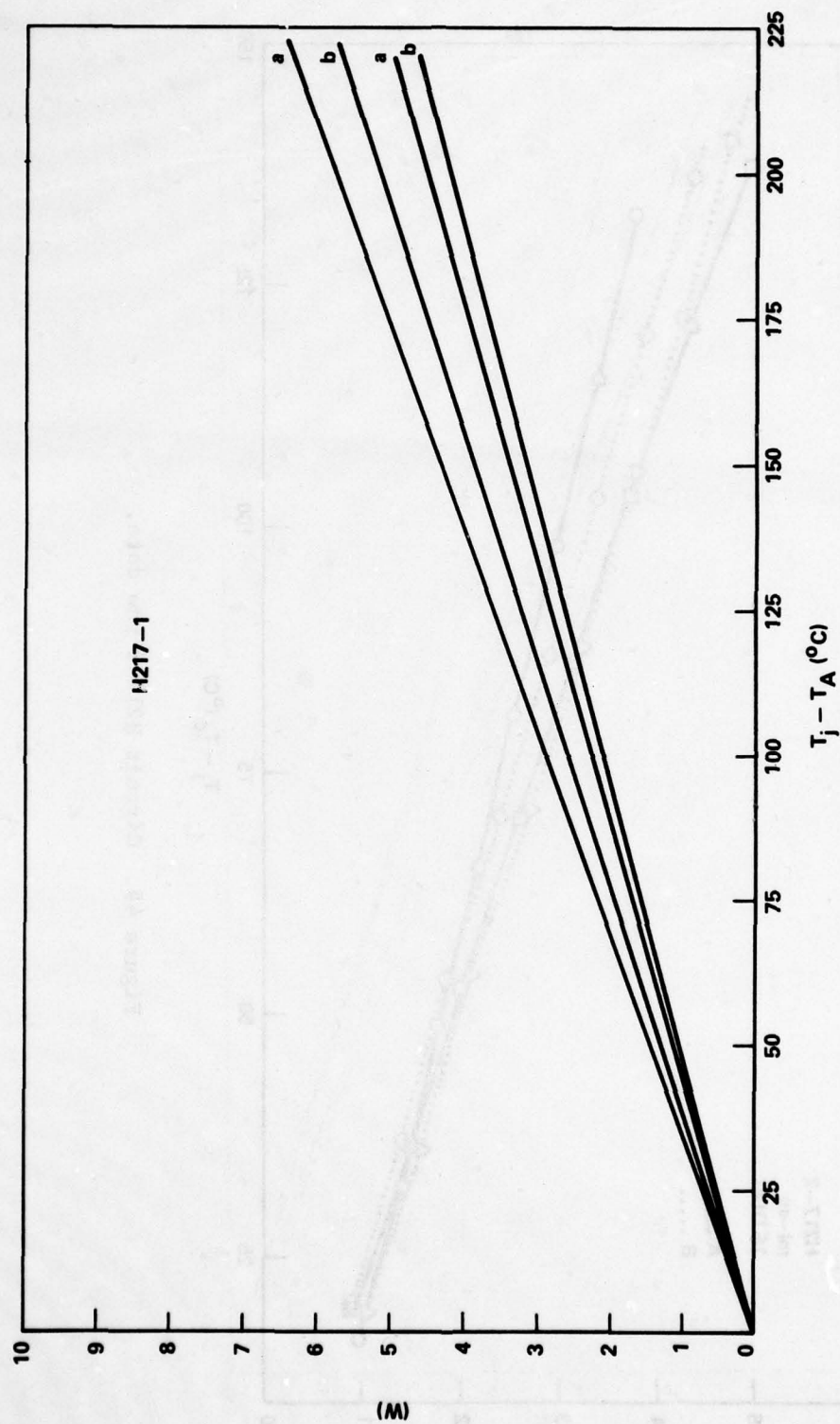


Figure 44. Circuit H217-1 junction to ambient.

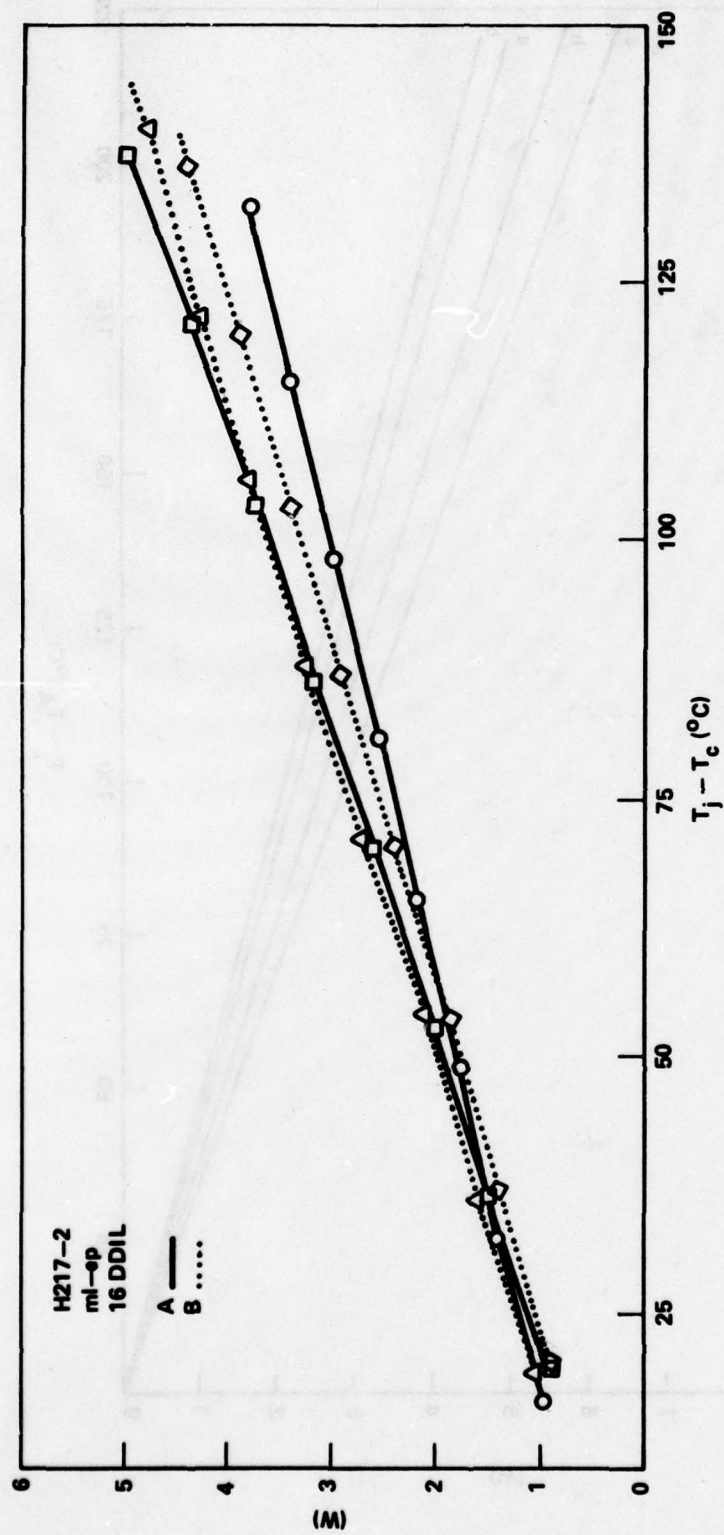


Figure 45. Circuit H217-2 raw data.

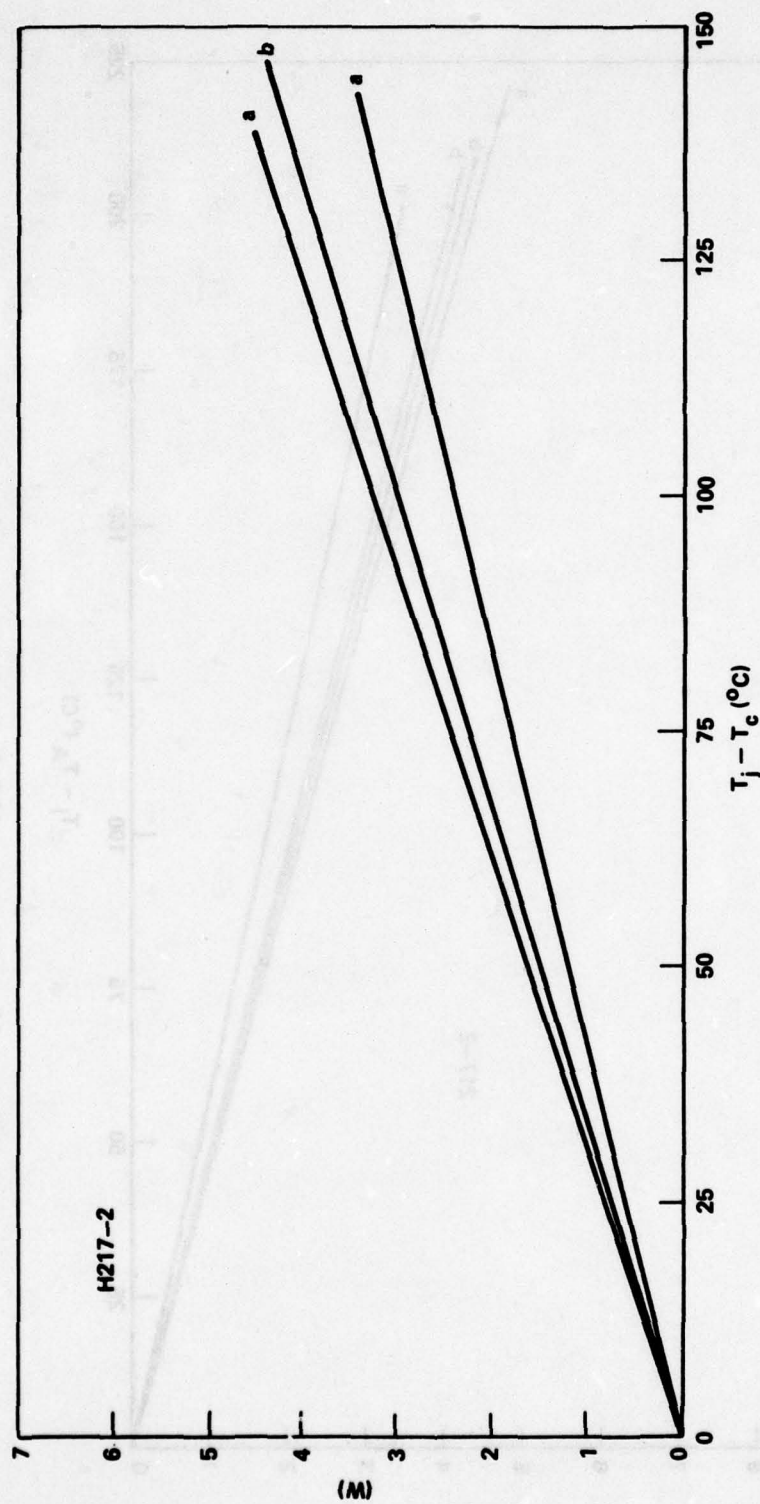


Figure 46. Circuit H217-2 junction to case.



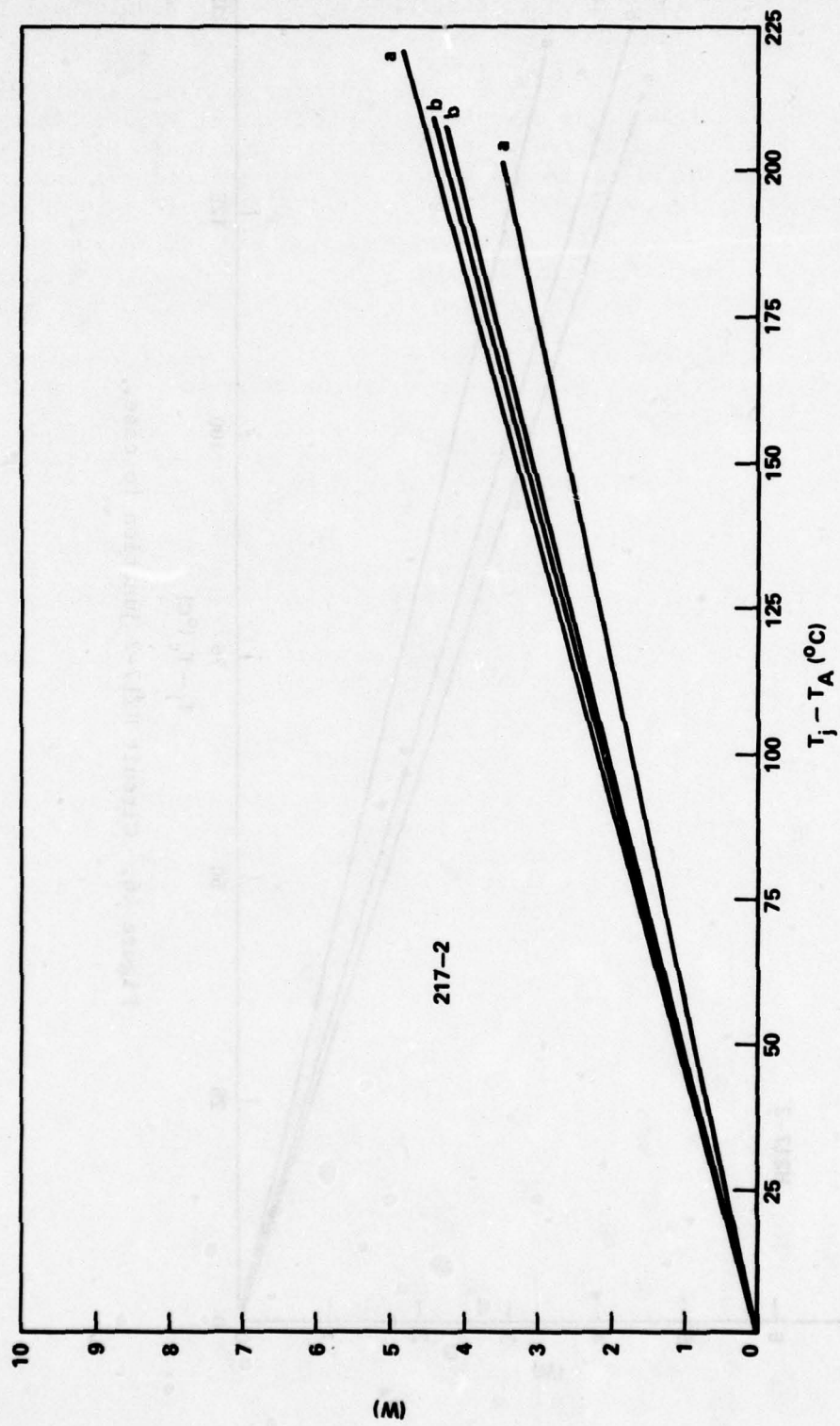


Figure 47. Circuit H217-2 junction to ambient.

#### 4. Thermal Characteristics of a 24-Pin Double Dual In-Line Package

The thermal impedance data for a 24-pin double-dual in-line package designated as circuit H216 are given in Figures 48 through 59. Figures 48, 49, and 50 are plots of the H216-3 circuit for the raw data (Figure 48), the normalized and averaged data (Figure 49), and the thermal impedance of junction to static ambient air  $\theta_{ja}$  (Figure 50).

This circuit (-3) was a eutectically mounted die, single layer substrate with the A parts substrate attached with electrically insulative epoxy (H-74) and the B parts substrate attached with H-417.

Figures 51, 52, and 53 are plots of the H216-4 circuit. Figure 51 presents the raw data. Figure 52 is the  $\theta_{jc}$  (normalized and linearized). Figure 53 is the thermal impedance of junction to static ambient air. This circuit (-4) was epoxy die mounted (H-4) single layer substrate with A parts H-74 attached and B parts H417 attached to the header.

Figures 54, 55, and 56 are the plots of the H 216-1 circuit. The raw data (Figure 54) and the normalized and averaged data (Figure 55) are of the thermal impedance of junction to case. The normalized and average data of the thermal impedance of the junction to static ambient air (Figure 56) are also presented. This circuit (-1) was a eutectically mounted die, multilayer substrate with the substrate to header bond via silver filled epoxy for Part B and H-74 for Part A.

Figures 57, 58, and 59 are the plots of the H216-2 circuit. The raw data (Figure 57) and the normalized and averaged data (Figure 58) are of the thermal impedance of junction to case. The normalized and averaged data of the thermal impedance of the junction to static ambient air (Figure 59) are also presented. This circuit (-2) was an epoxy mounted die, multilayer substrate with the substrate to header bond of H-74 in Type A parts and H-417 in Type B parts.

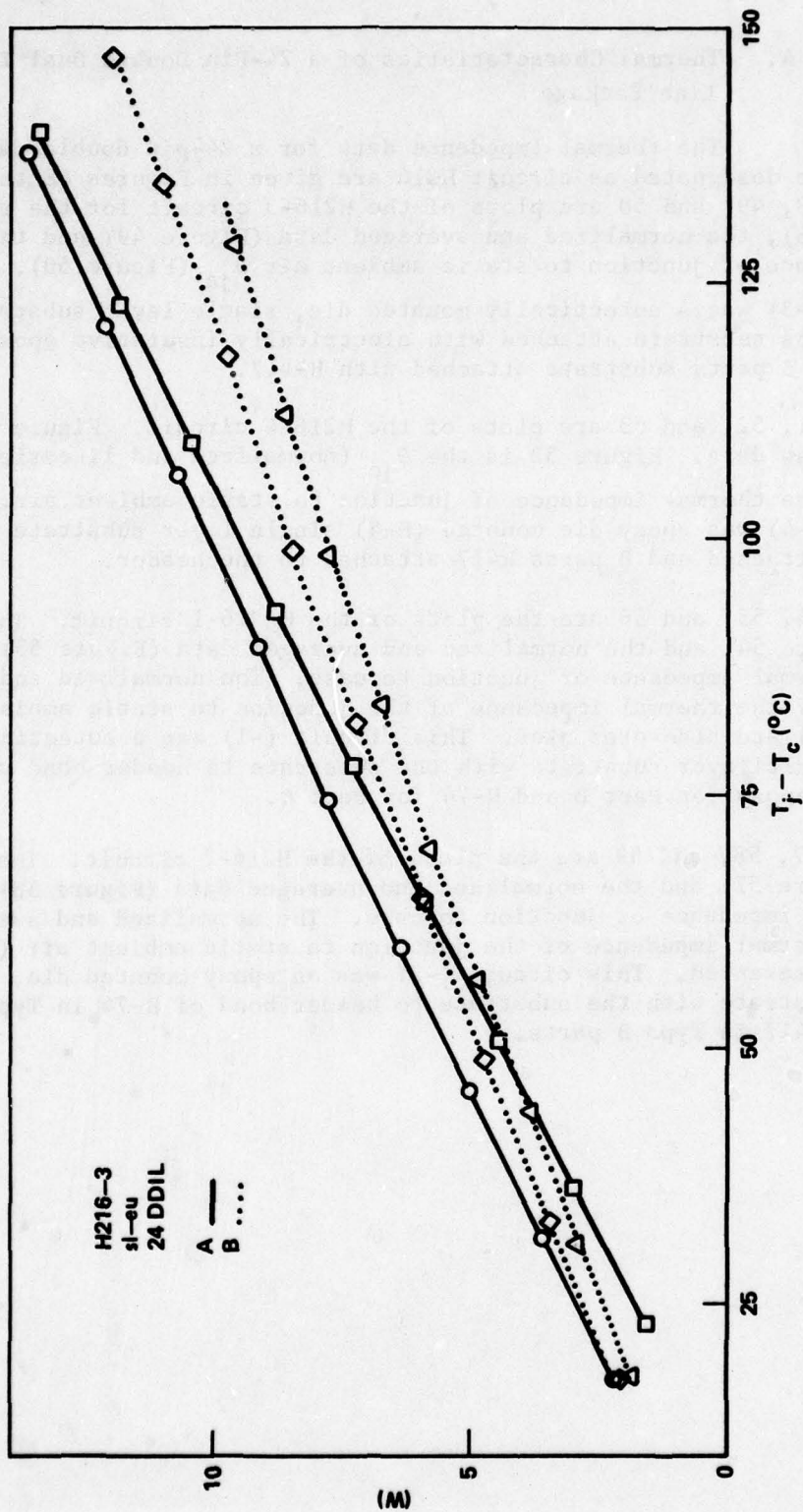


Figure 48. Circuit H216-3 raw data.



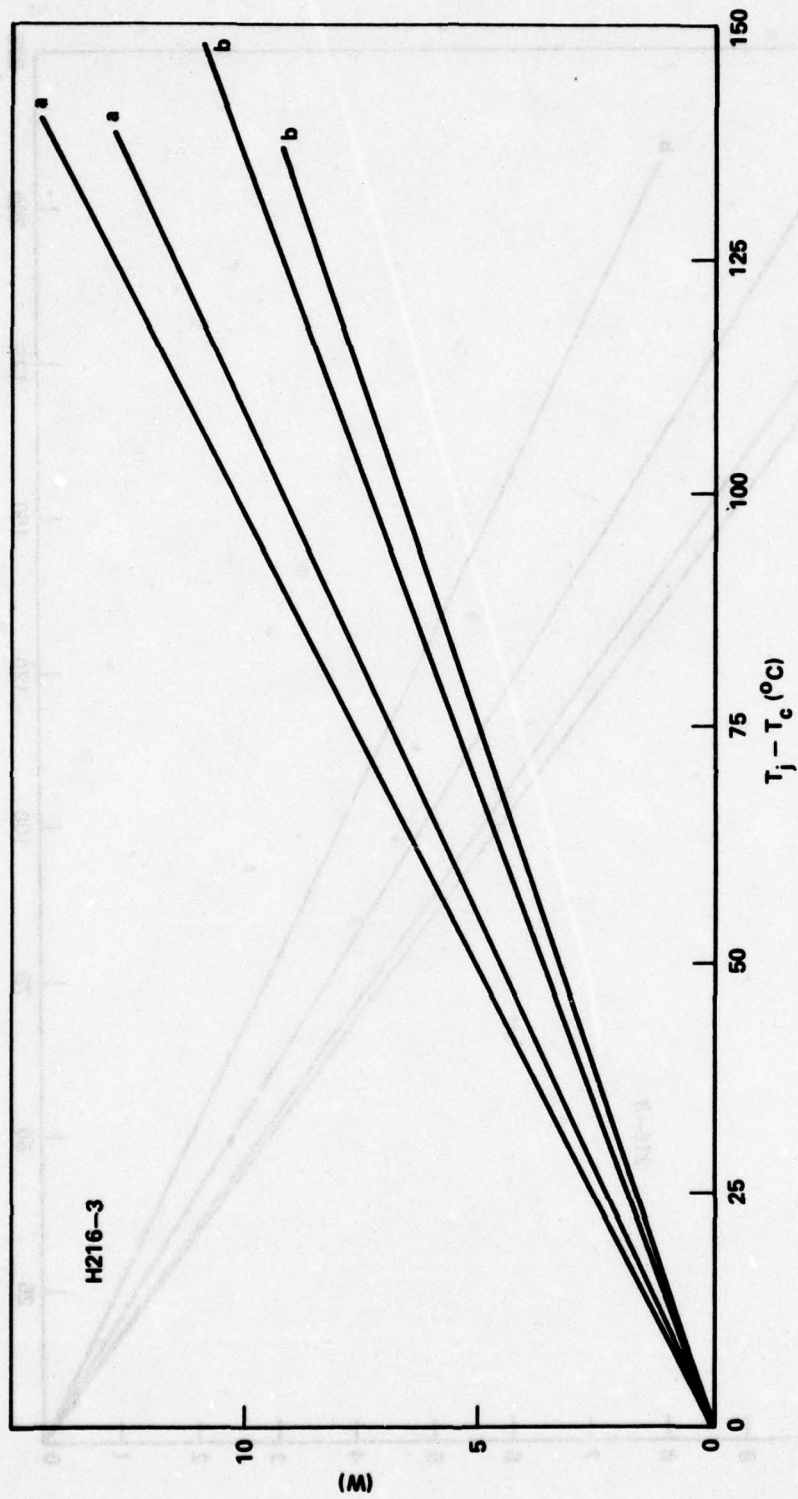


Figure 49. Circuit H216-3 junction to case.

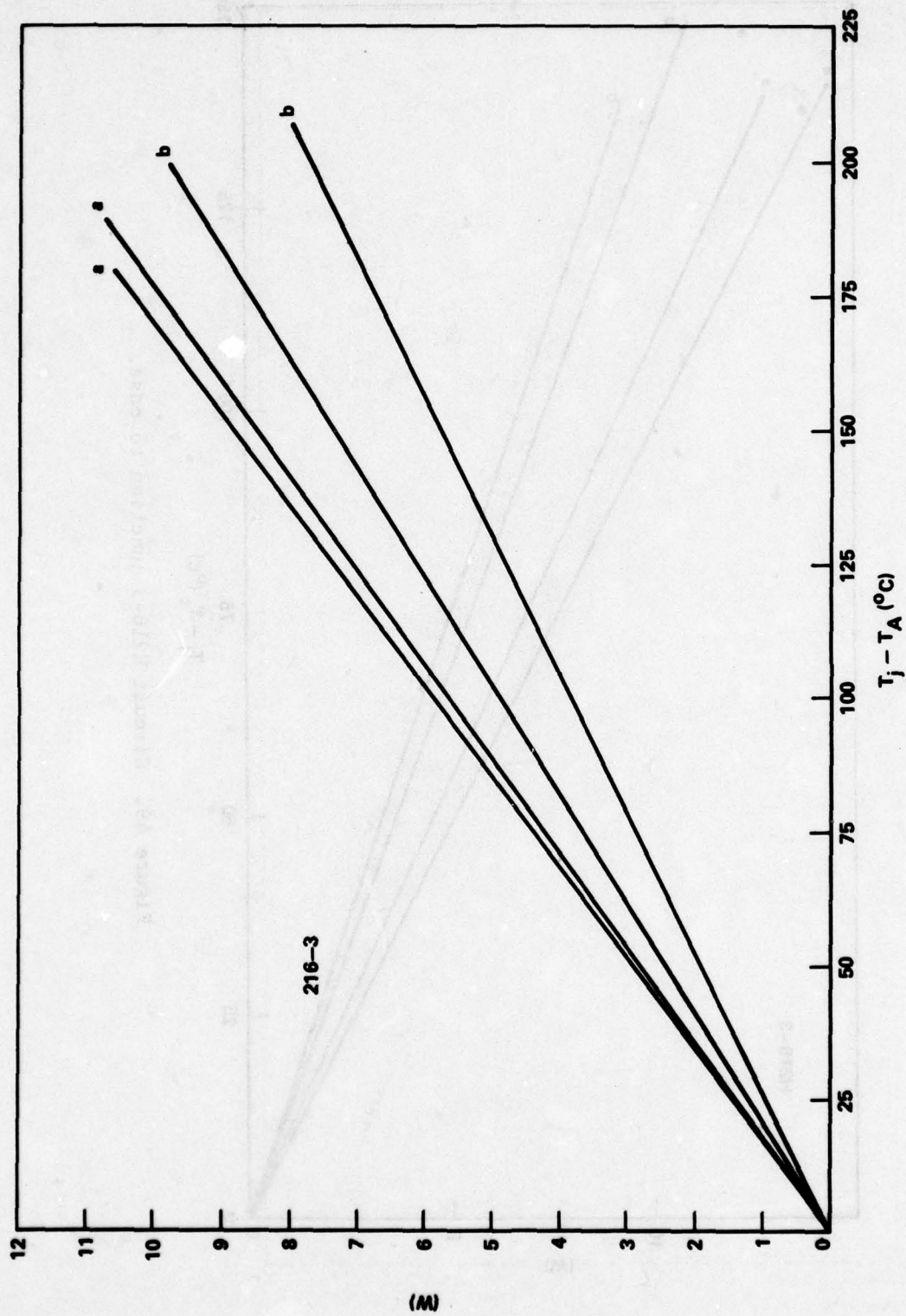


Figure 50. Circuit H216-3 junction to ambient.

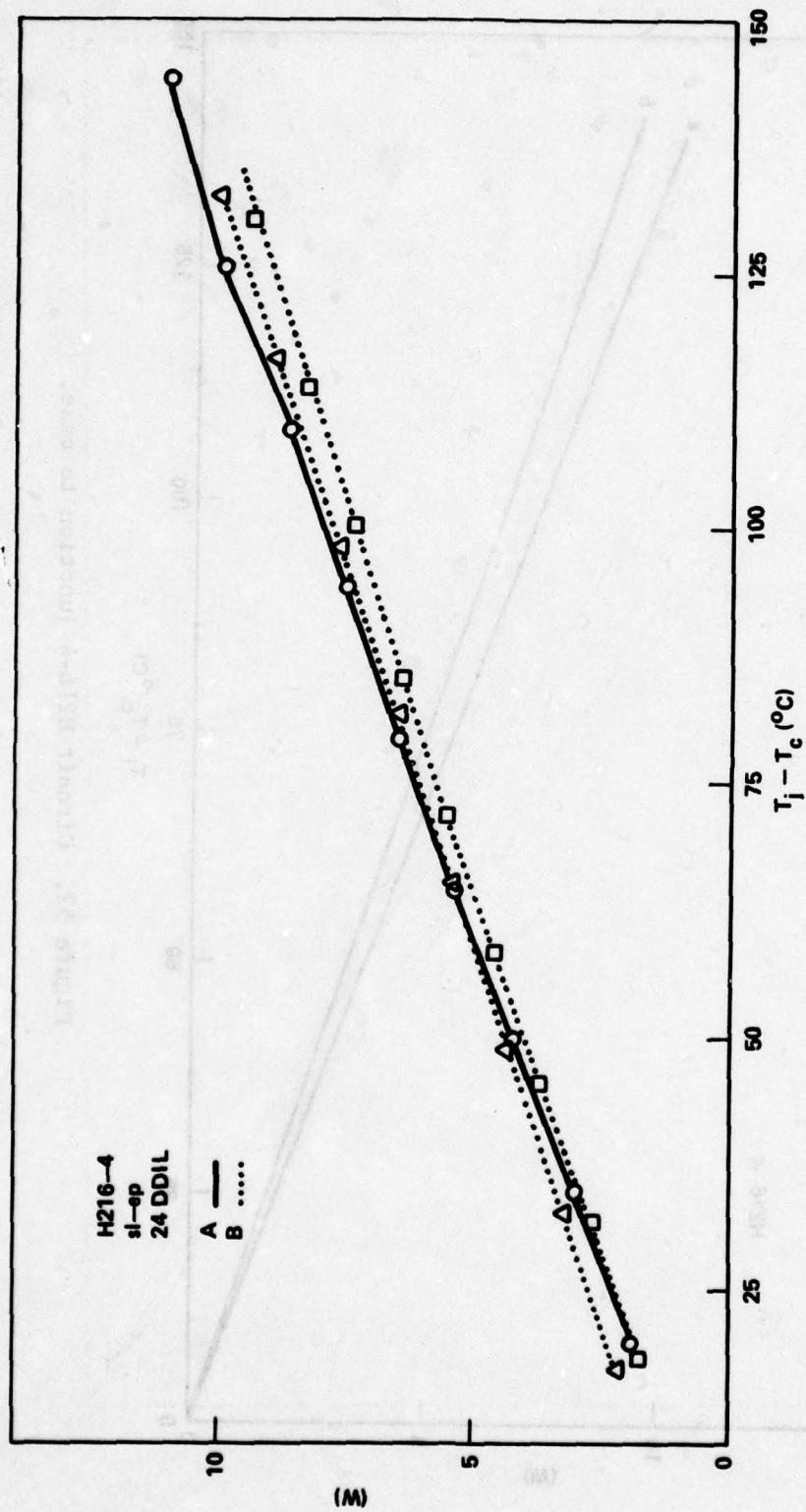


Figure 51. Circuit H216-4 raw data.



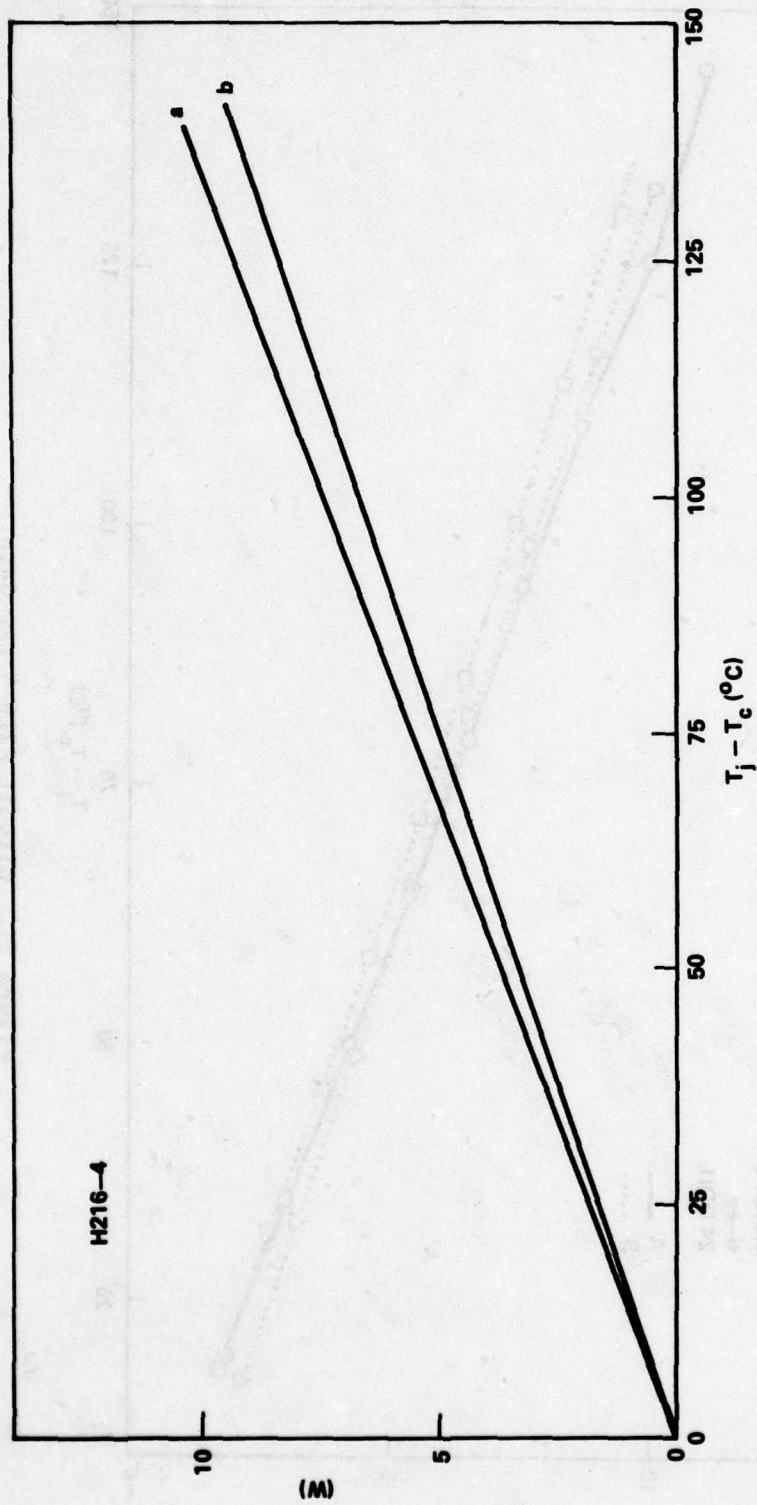


Figure 52. Circuit H216-4 junction to case.

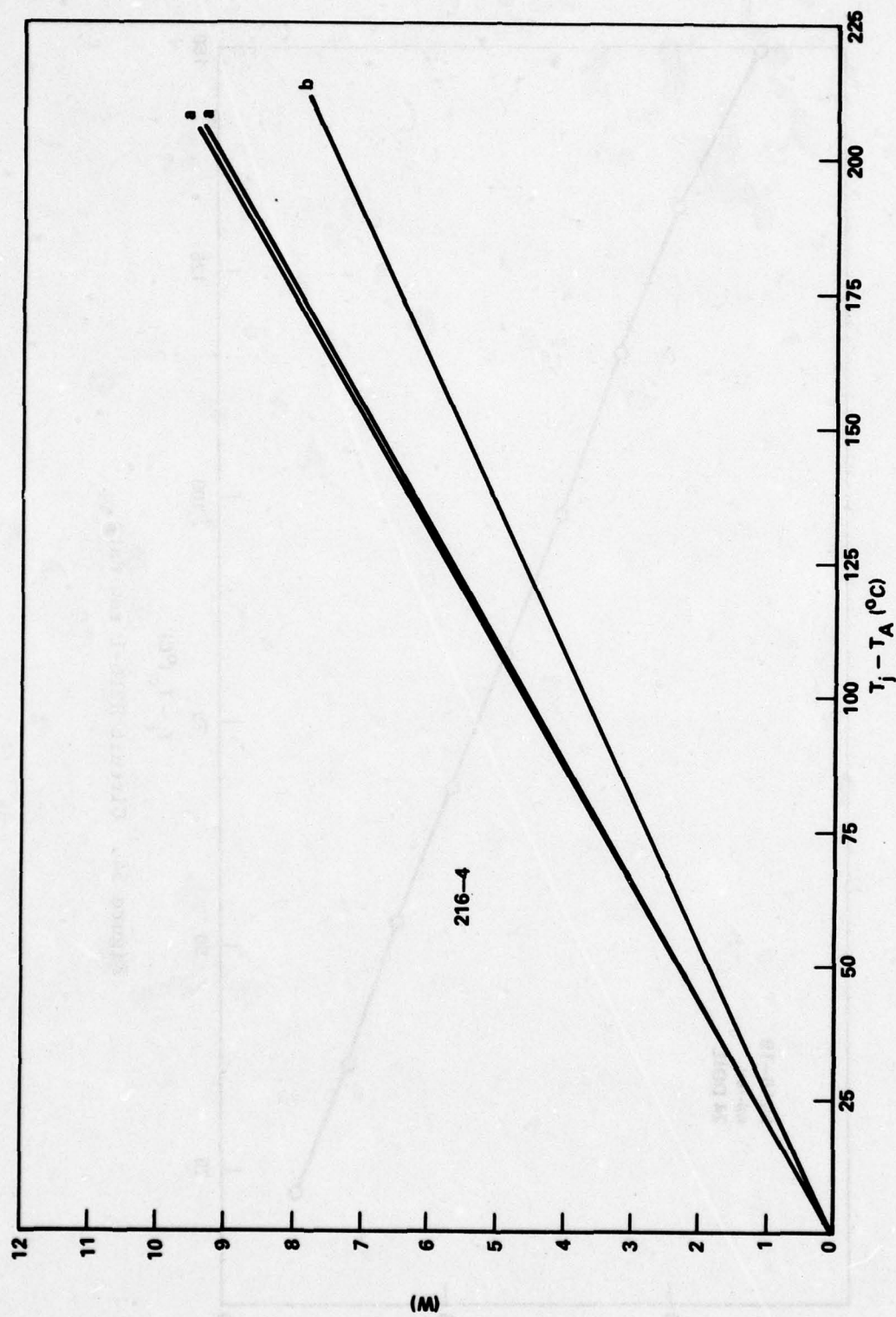


Figure 53. Circuit H216-4 junction to ambient.

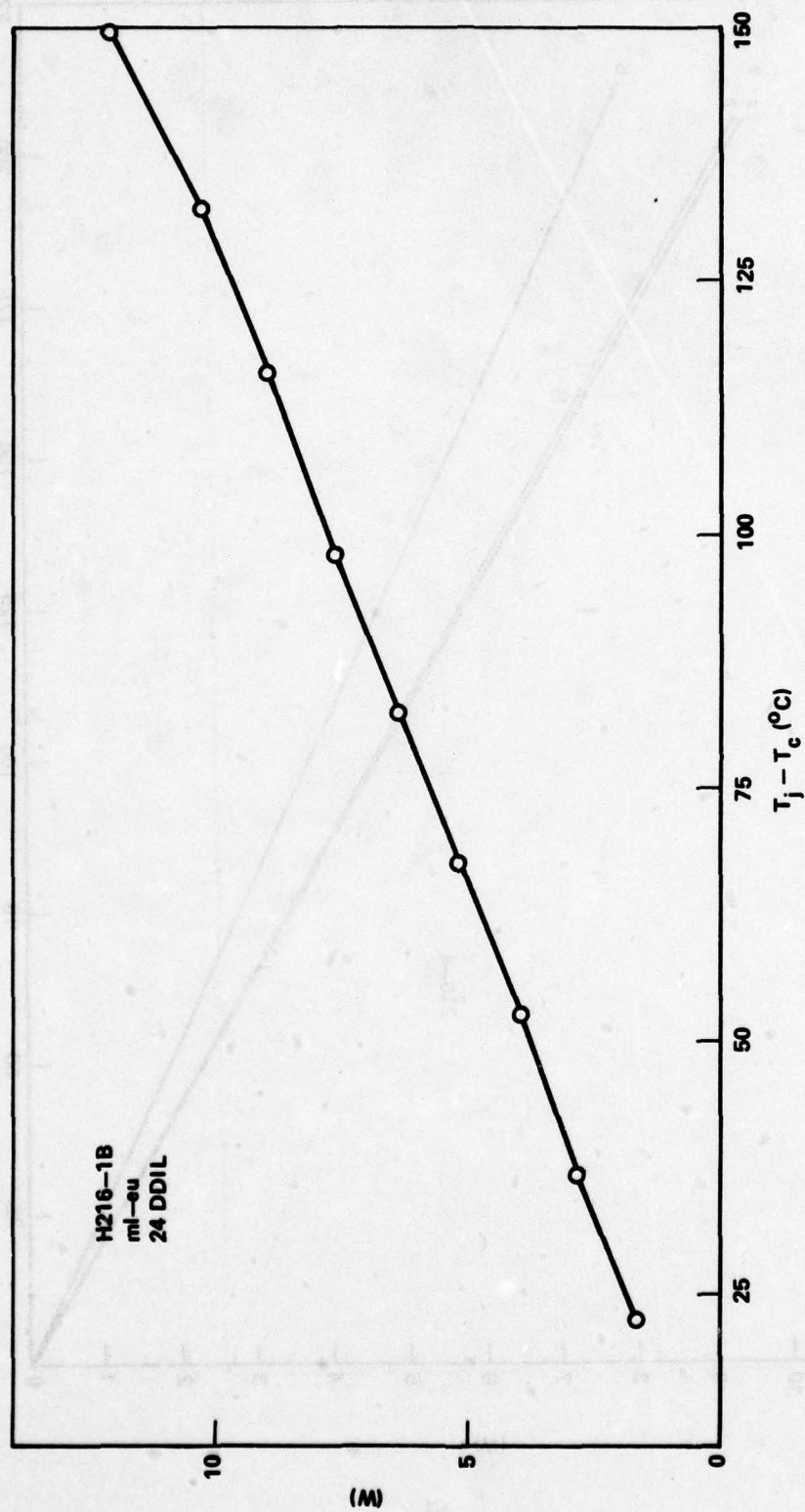


Figure 54. Circuit H216-1 raw data.



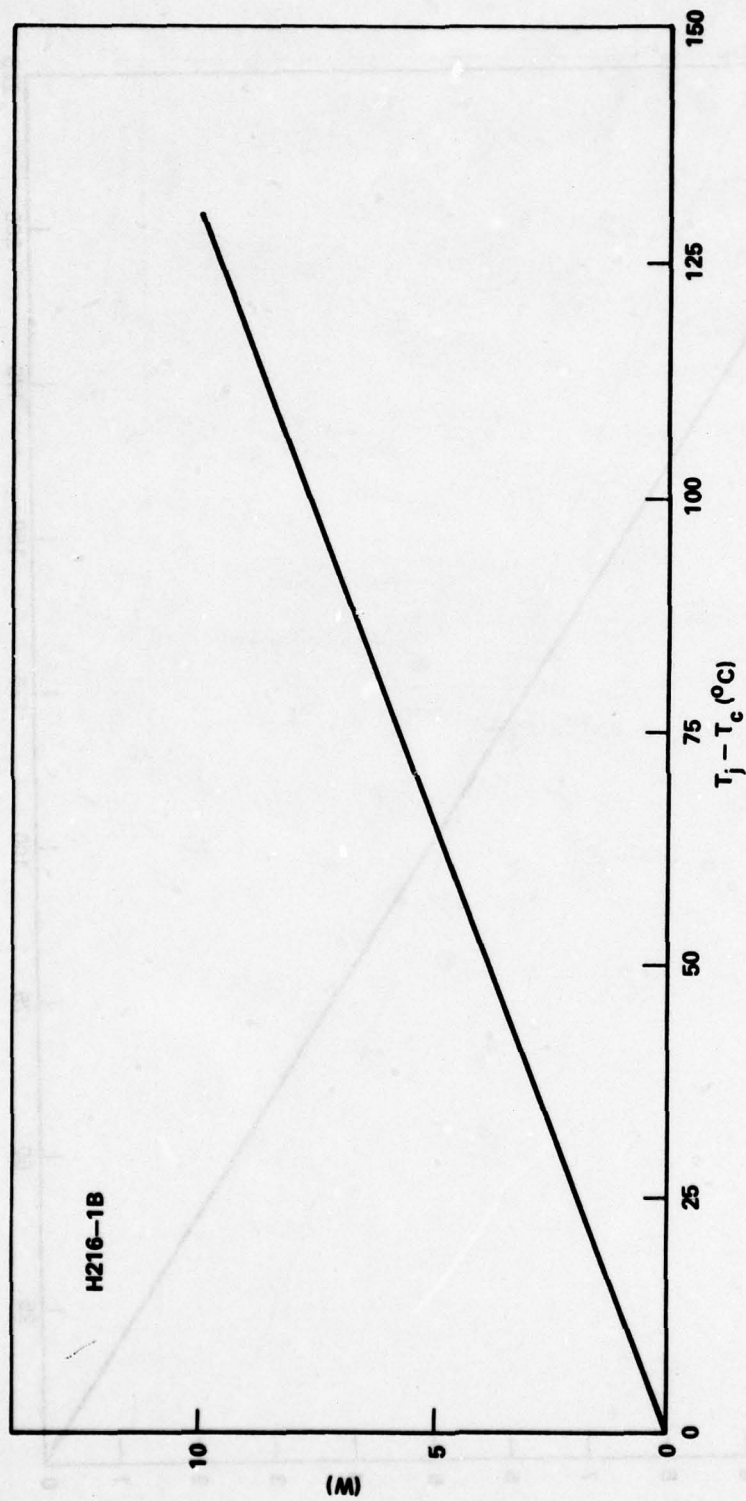


Figure 55. Circuit H216-1 junction to case.

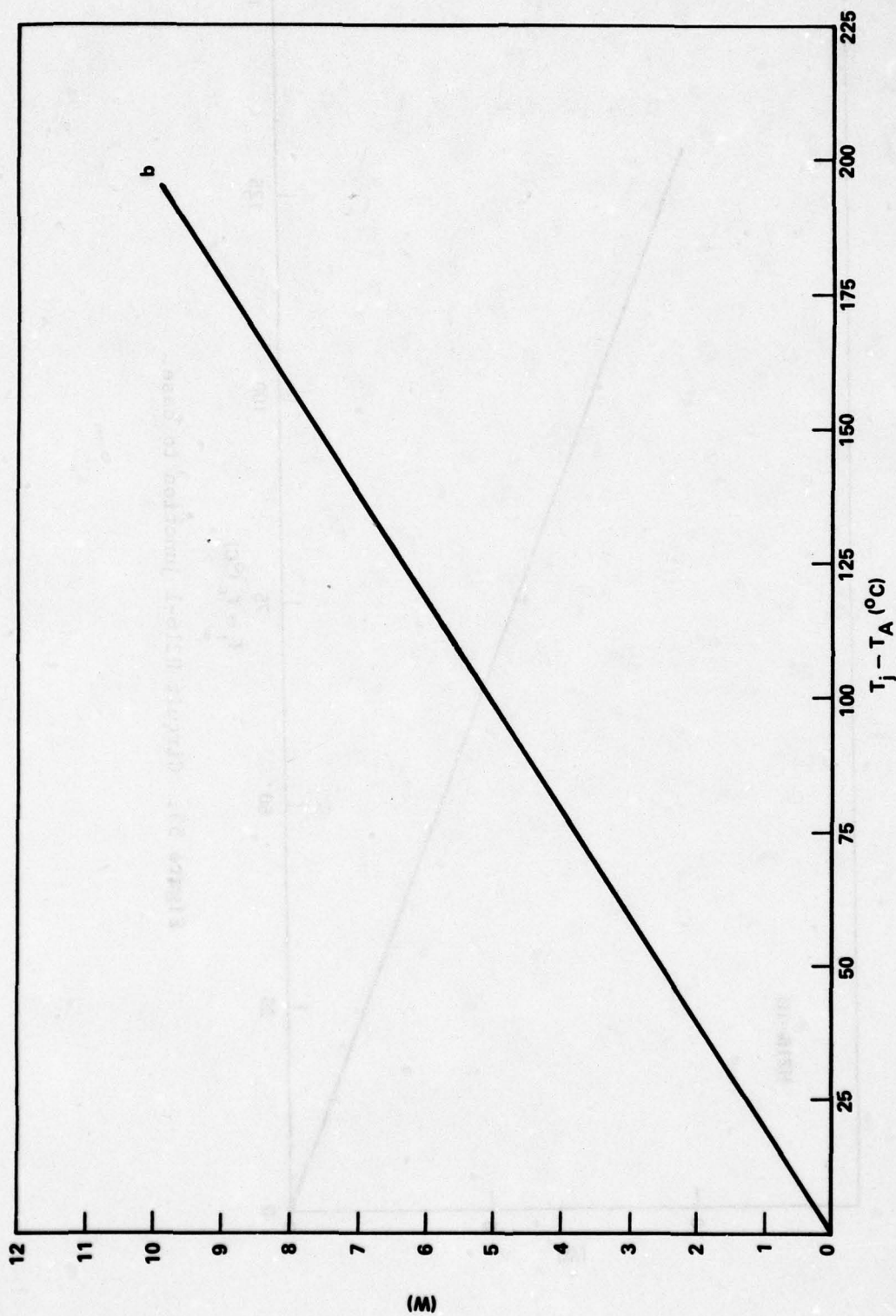


Figure 56. Circuit H216-1 junction to ambient.

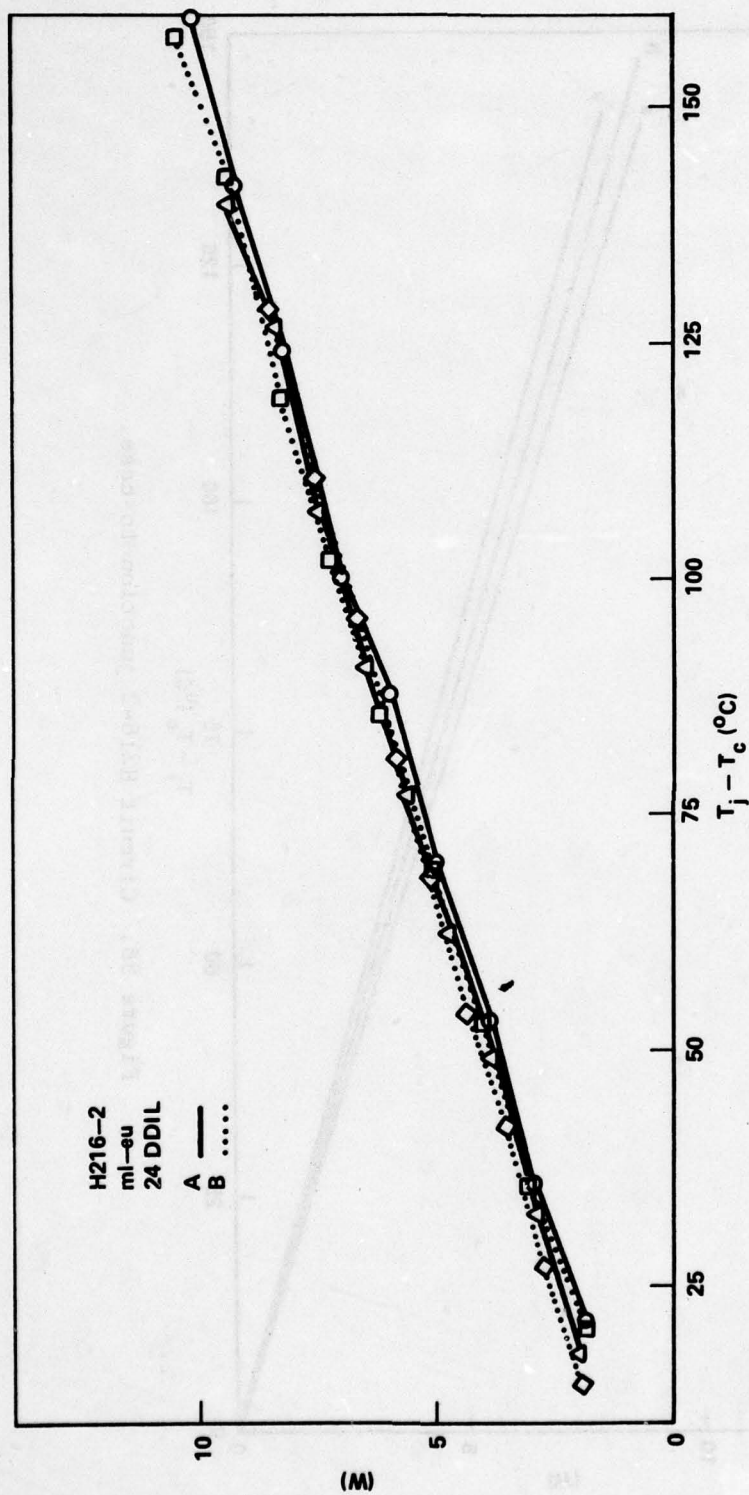


Figure 57. Circuit H216-2 raw data.



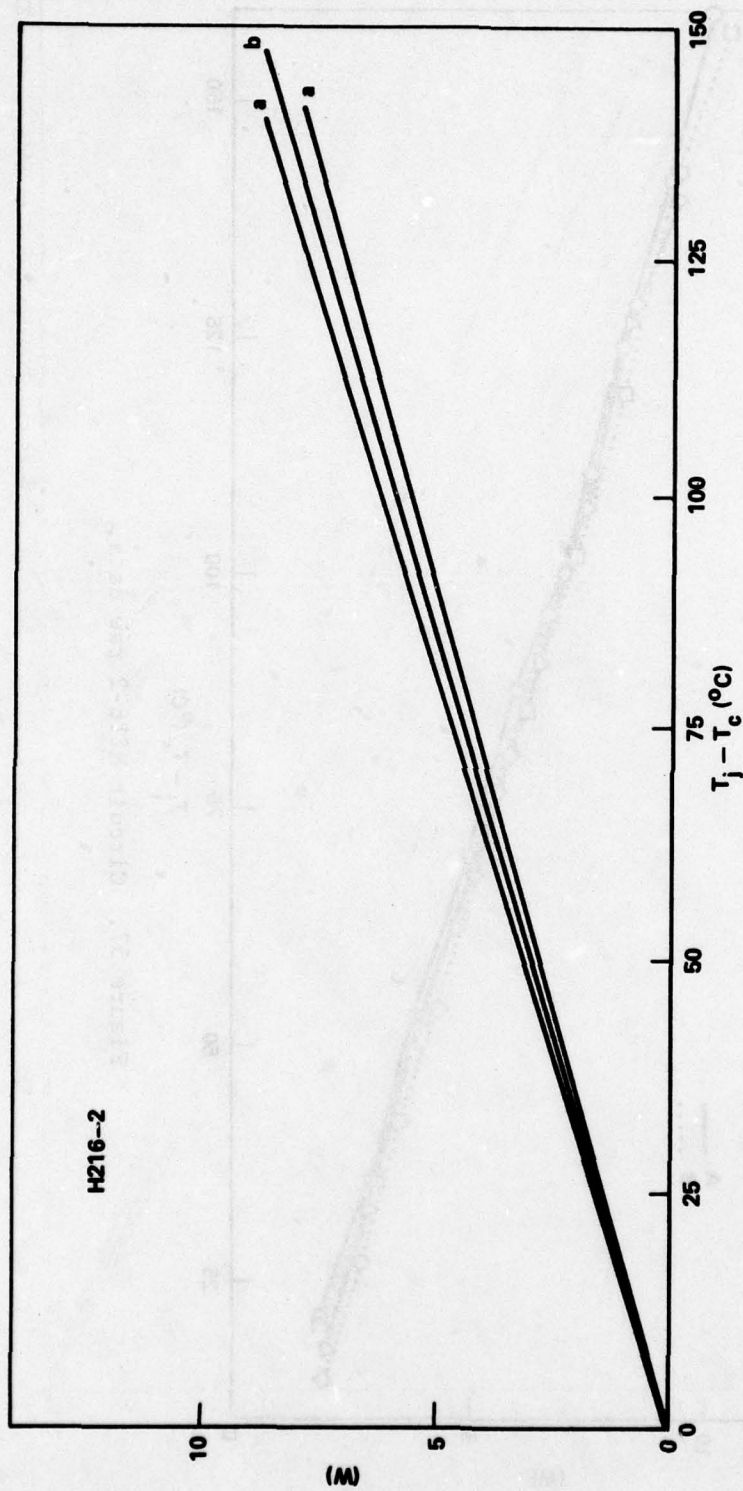


Figure 58. Circuit H216-2 junction to case.

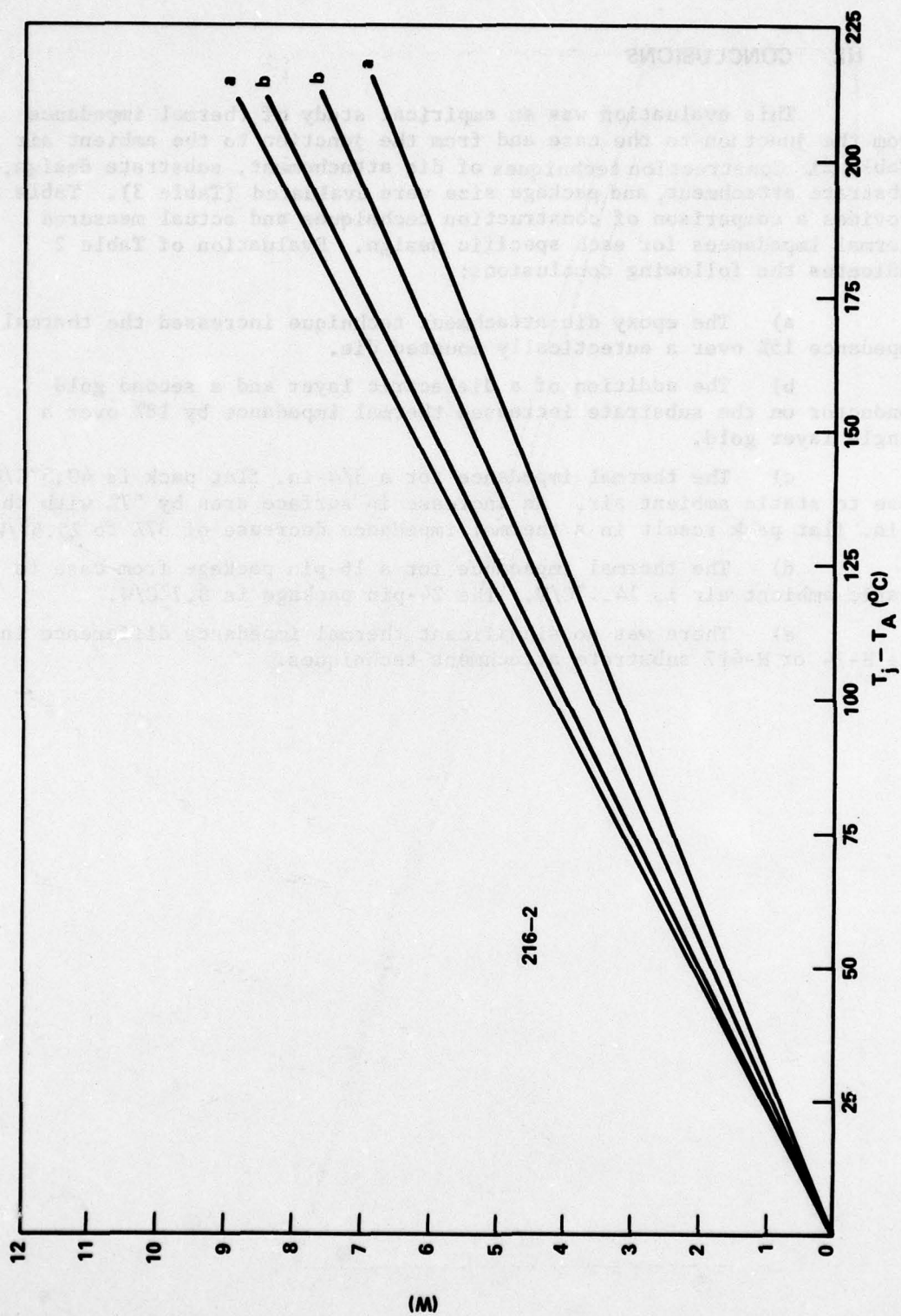


Figure 59. Circuit H215-2 junction to ambient.

### III. CONCLUSIONS

This evaluation was an empirical study of thermal impedance from the junction to the case and from the junction to the ambient air (Table 2). Construction techniques of die attachment, substrate design, substrate attachment, and package size were evaluated (Table 3). Table 2 provides a comparison of construction techniques and actual measured thermal impedances for each specific design. Evaluation of Table 2 indicates the following conclusions:

- a) The epoxy die attachment technique increased the thermal impedance 15% over a eutectically mounted die.
- b) The addition of a dielectric layer and a second gold conductor on the substrate increased thermal impedance by 18% over a single layer gold.
- c) The thermal impedance for a 3/4-in. flat pack is 40.5°C/W case to static ambient air. An increase in surface area by 57% with the 1-in. flat pack result in a thermal impedance decrease of 37% to 25.5°C/W.
- d) The thermal impedance for a 16-pin package from case to static ambient air is 14.1°C/W. The 24-pin package is 8.7°C/W.
- e) There was no significant thermal impedance difference in the H-74 or H-417 substrate attachment techniques.



TABLE 2. CONSTRUCTION TECHNIQUE AND THERMAL IMPEDANCE

| Package Type      | Construction Technique |       |                |       |                  |             | Thermal Impedance Junction to Case (°C/watt) | Thermal Impedance Junction to Ambient (°C/watt) |
|-------------------|------------------------|-------|----------------|-------|------------------|-------------|--|---|
|                   | Substrate Attachment   |       | Die Attachment |       | Substrate Design |             |  |   |
|                   |                        |       |                |       |                  |             |  |   |
|                   | H-74*                  | H417* | Eutectic       | Epoxy | Single Layer     | Multi Layer |  |   |
| 3/4-in. Flat Pack |                        | x     | x              |       | x                |             | 21.8   | 62.5  |
|                   |                        | x     |                | x     | x                |             | 27.2   | 67.5  |
|                   |                        | x     | x              |       |                  | x           | 31.0   | 71.8  |
|                   |                        | x     |                | x     |                  | x           | 34.6   | 74.7  |
| 1-in. flat pack   |                        | x     | x              |       | x                |             | 11.0   | 40.5  |
|                   |                        | x     |                | x     | x                |             | 12.7   | 36.8  |
|                   |                        | x     | x              |       |                  | x           | 13.4   | 35.7  |
|                   |                        | x     |                | x     |                  | x           | 13.0   | 38.1  |
| 16-pin DDIL       | x                      |       | x              |       | x                |             | 22.0   | 39.8  |
|                   |                        | x     | x              |       | x                |             | 19.7   | 34.8  |
|                   | x                      |       |                | x     | x                |             | 27.0   | 41.6  |
|                   |                        | x     |                | x     | x                |             | 27.0   | 35.5  |
|                   | x                      |       | x              |       |                  | x           | 28.1   | 41.1  |
|                   |                        | x     | x              |       |                  | x           | 29.3   | 41.5  |
|                   | x                      |       |                | x     |                  | x           | 36.3   | 52.9  |
|                   |                        |       | x              |       | x                | 33.5        | 48.6   |   |
| 23-Pin DDIL       | x                      |       | x              |       | x                |             | 10.4   | 17.2  |
|                   |                        | x     | x              |       | x                |             | 14.3   | 23.1  |
|                   | x                      |       |                | x     | x                |             | 13.5   | 24.5  |
|                   |                        | x     |                | x     | x                |             | 15.0   | 21.7  |
|                   |                        | x     | x              |       |                  |             | 13.0   | 19.8  |
|                   | x                      |       |                | x     |                  |             | 17.0   | 26.4  |
|                   |                        |       | x              |       | x                | 16.9        | 27.6   |   |

\*Note: H-74 is electrically insulative and thermally conductive epoxy.  
H417 is silver filled epoxy.

TABLE 3. CONSTRUCTION TECHNIQUE AND MAXIMUM POWER DISSIPATION

| Package Type      | Construction Technique |       |                |       |                  | Maximum Power Dissipation                       |                                |                                       |
|-------------------|------------------------|-------|----------------|-------|------------------|---|--------------------------------|---------------------------------------|
|                   | Substrate Attachment   |       | Die Attachment |       | Substrate Design | Infinite Heat Sink<br>$T_j = 175^\circ\text{C}$ |                                | Free Air<br>$T_j = 175^\circ\text{C}$ |
|                   | H-74*                  | H417* | Eutectic       | Epoxy | Single Layer     | Multi Layer                                     | (W)<br>$T = 125^\circ\text{C}$ | (W)<br>$T = 85^\circ\text{C}$         |
| 3/4-in. Flat Pack |                        | x     | x              | x     | x                |   | 2.3                            | 4.1                                   |
|                   |                        | x     |                |       | x                |   | 1.8                            | 3.3                                   |
|                   |                        | x     | x              |       |                  | x   | 1.6                            | 2.9                                   |
|                   |                        | x     |                | x     |                  | x   | 1.4                            | 2.6                                   |
| 1-in. Flat Pack   |                        | x     | x              |       | x                |   | 4.5                            | 8.2                                   |
|                   |                        | x     |                | x     | x                |   | 3.9                            | 7.1                                   |
|                   |                        | x     | x              |       |                  | x   | 3.7                            | 6.7                                   |
|                   |                        | x     |                | x     |                  | x   | 3.8                            | 6.9                                   |
| 16-Pin DDIL       | x                      | x     | x              |       | x                |   | 2.3                            | 4.1                                   |
|                   |                        | x     | x              |       | x                |   | 2.5                            | 4.6                                   |
|                   | x                      |       |                | x     | x                |   | 1.9                            | 3.3                                   |
|                   |                        | x     |                | x     | x                |   | 1.9                            | 3.3                                   |
|                   | x                      |       | x              |       |                  | x   | 1.8                            | 3.2                                   |
|                   |                        | x     | x              |       | x                | x   | 1.7                            | 3.1                                   |
|                   | x                      |       |                | x     |                  | x   | 1.4                            | 2.5                                   |
|                   |                        | x     |                | x     |                  | x   | 1.5                            | 2.7                                   |
|                   |                        |       |                |       |                  |   | 4.8                            | 8.6                                   |
|                   |                        | x     | x              |       | x                |   | 3.5                            | 6.3                                   |
| 24-Pin DDIL       | x                      |       |                |       | x                |   | 3.7                            | 6.7                                   |
|                   | x                      |       |                | x     | x                |   | 3.3                            | 6.0                                   |
|                   |                        | x     |                | x     |                  | x   | 3.8                            | 6.9                                   |
|                   | x                      |       | x              |       | x                |   | 2.9                            | 5.3                                   |
|                   |                        | x     |                | x     |                  | x   | 3.0                            | 5.3                                   |
|                   |                        |       |                |       |                  |   | 2.9                            | 5.2                                   |

\*Note: H-74 is electrically insulative and thermally conductive epoxy  
H-417 is silver filled epoxy

# Appendix. RAW DATA FROM EXPERIMENTAL MEASUREMENT

| H 214-1        |                                | SN 001         |                                |        | SN 002         |                                |        | SN 003         |                                |        |
|----------------|--------------------------------|----------------|--------------------------------|--------|----------------|--------------------------------|--------|----------------|--------------------------------|--------|
| T <sub>a</sub> | T <sub>j</sub> -T <sub>a</sub> | T <sub>c</sub> | T <sub>j</sub> -T <sub>c</sub> | (W)    | T <sub>c</sub> | T <sub>j</sub> -T <sub>c</sub> | (W)    | T <sub>c</sub> | T <sub>j</sub> -T <sub>c</sub> | (W)    |
| -55            | 230                            | 86.3           | 88.7                           | 7.431  | 80.2           | 94.8                           | 7.199  | 89.8           | 85.2                           | 7.594  |
| -25            | 200                            | 98.2           | 76.8                           | 6.549  | 91.6           | 83.4                           | 6.316  | 98.8           | 76.2                           | 6.883  |
| 0              | 175                            | 106.8          | 68.2                           | 5.845  | 100.1          | 74.9                           | 5.703  | 108.8          | 62.2                           | 6.085  |
| 25             | 150                            | 116.8          | 58.2                           | 5.140  | 110.8          | 64.2                           | 4.962  | 118.3          | 56.7                           | 5.333  |
| 50             | 125                            | 125.4          | 49.6                           | 4.446  | 119.1          | 55.9                           | 4.343  | 125.9          | 49.1                           | 4.683  |
| 75             | 100                            | 134.4          | 40.6                           | 3.772  | 129.2          | 45.8                           | 3.645  | 135.6          | 39.4                           | 3.896  |
| 100            | 75                             | 142.6          | 32.4                           | 3.153  | 138.4          | 36.6                           | 3.056  | 143.6          | 31.4                           | 3.278  |
| 125            | 50                             | 152.5          | 22.5                           | 2.430  | 148.7          | 26.3                           | 2.383  | 152.5          | 22.5                           | 2.582  |
| 150            | 25                             | 163.5          | 11.5                           | 1.740  | 159.3          | 15.7                           | 1.664  | 162.4          | 12.6                           | 1.789  |
| H 214-2        |                                | SN 004         |                                |        | SN 005         |                                |        | SN 006         |                                |        |
| T <sub>a</sub> | T <sub>j</sub> -T <sub>a</sub> | T <sub>c</sub> | T <sub>j</sub> -T <sub>c</sub> | (W)    | T <sub>c</sub> | T <sub>j</sub> -T <sub>c</sub> | (W)    | T <sub>c</sub> | T <sub>j</sub> -T <sub>c</sub> | (W)    |
| -55            | 230                            | 70.7           | 104.3                          | 6.054  | 82.7           | 92.3                           | 7.054  | 76.9           | 98.1                           | 7.039  |
| -25            | 200                            | 89.8           | 85.2                           | 6.204  | 92.8           | 82.2                           | 6.246  | 87.9           | 87.1                           | 6.339  |
| 0              | 175                            | 100.4          | 74.6                           | 5.496  | 102.2          | 72.8                           | 5.591  | 99.5           | 75.5                           | 5.679  |
| 25             | 150                            | 110.9          | 64.1                           | 4.807  | 113.0          | 62.0                           | 4.842  | 110.8          | 64.2                           | 4.997  |
| 50             | 125                            | 119.7          | 55.3                           | 4.215  | 121.1          | 53.9                           | 4.272  | 122.0          | 53.0                           | 4.393  |
| 75             | 100                            | 129.7          | 45.3                           | 3.554  | 130.3          | 44.7                           | 3.638  | 131.4          | 43.6                           | 3.753  |
| 100            | 75                             | 140.0          | 35.0                           | 2.930  | 139.8          | 35.2                           | 2.974  | 141.05         | 33.95                          | 3.110  |
| 125            | 50                             | 149.1          | 25.9                           | 2.282  | 149.3          | 25.7                           | 2.337  | 151.05         | 23.95                          | 2.460  |
| 150            | 25                             |                |                                | 1.6316 | 159.6          | 15.4                           | 1.6383 | 162.0          | 13.0                           | 1.7236 |
| H 214-3        |                                | SN 007         |                                |        | SN 008         |                                |        | SN 009         |                                |        |
| T <sub>a</sub> | T <sub>j</sub> -T <sub>a</sub> | T <sub>c</sub> | T <sub>j</sub> -T <sub>c</sub> | (W)    | T <sub>c</sub> | T <sub>j</sub> -T <sub>c</sub> | (W)    | T <sub>c</sub> | T <sub>j</sub> -T <sub>c</sub> | (W)    |
| -55            | 230                            | 97.5           | 77.5                           | 8.151  | 100.5          | 74.5                           | 7.869  | 93.0           | 82.0                           | 7.787  |
| -25            | 200                            | 108.4          | 66.6                           | 7.176  | 110.1          | 64.9                           | 6.873  | 103.9          | 71.1                           | 6.903  |
| 0              | 175                            | 118.8          | 56.6                           | 6.463  | 118.2          | 56.8                           | 6.241  | 111.75         | 57.25                          | 6.190  |
| 25             | 150                            | 128.0          | 47.0                           | 5.665  | 125.6          | 49.4                           | 5.463  | 121.8          | 53.2                           | 5.393  |
| 50             | 125                            | 135.4          | 39.6                           | 4.906  | 132.5          | 42.5                           | 4.696  | 129.8          | 45.2                           | 4.673  |
| 75             | 100                            | 142.6          | 32.4                           | 4.148  | 139.7          | 35.3                           | 3.973  | 137.6          | 37.4                           | 4.026  |
| 100            | 75                             | 150.0          | 25.0                           | 3.397  | 146.0          | 29.0                           | 3.385  | 146.0          | 29.0                           | 3.330  |
| 125            | 50                             | 157.1          | 17.9                           | 2.701  | 154.9          | 20.1                           | 2.520  | 154.0          | 21.0                           | 2.526  |
| 150            | 25                             | 164.5          | 10.5                           | 1.840  | 164.05         | 10.95                          | 1.851  | 163.4          | 11.6                           | 1.858  |
| H-214-4        |                                | SN 010         |                                |        | SN 011         |                                |        | SN 012         |                                |        |
| T <sub>a</sub> | T <sub>j</sub> -T <sub>a</sub> | T <sub>c</sub> | T <sub>j</sub> -T <sub>c</sub> | (W)    | T <sub>c</sub> | T <sub>j</sub> -T <sub>c</sub> | (W)    | T <sub>c</sub> | T <sub>j</sub> -T <sub>c</sub> | (W)    |
| -55            | 230                            | 76.4           | 98.6                           | 7.086  | 90.9           | 84.1                           | 7.774  | 92.9           | 82.1                           | 7.580  |
| -25            | 200                            | 88.2           | 86.8                           | 6.247  | 101.8          | 73.2                           | 6.888  | 103.7          | 71.3                           | 6.730  |
| 0              | 175                            | 97.6           | 77.4                           | 5.569  | 111.9          | 63.1                           | 6.122  | 112.3          | 62.7                           | 6.076  |
| 25             | 150                            | 106.3          | 68.7                           | 4.947  | 119.3          | 55.7                           | 5.465  | 121.4          | 53.6                           | 5.368  |
| 50             | 125                            | 117.3          | 57.7                           | 4.205  | 128.2          | 46.8                           | 4.693  | 130.05         | 45.0                           | 4.603  |
| 75             | 100                            | 126.8          | 48.2                           | 3.541  | 136.6          | 38.4                           | 4.037  | 137.9          | 37.1                           | 3.996  |
| 100            | 75                             | 135.6          | 39.4                           | 2.913  | 145.9          | 29.1                           | 3.265  | 147.6          | 27.4                           | 3.247  |
| 125            | 50                             | 145.7          | 29.3                           | 2.247  | 153.3          | 21.7                           | 2.656  | 156.0          | 19.0                           | 2.519  |
| 150            | 25                             | 156.0          | 19.0                           | 1.557  | 163.5          | 11.5                           | 1.8592 | 164.4          | 10.6                           | 1.869  |



| H-215-1 |             | SN 001 |             |        | SN 002 |             |        | SN 003 |             |        |
|---------|-------------|--------|-------------|--------|--------|-------------|--------|--------|-------------|--------|
| $T_a$   | $T_j - T_a$ | $T_c$  | $T_j - T_c$ | (W)    | $T_c$  | $T_j - T_c$ | (W)    | $T_c$  | $T_j - T_c$ | (W)    |
| -55     | 230         | 74.2   | 100.8       | 3.792  | 52.6   | 122.4       | 3.351  | 81.1   | 93.9        | 3.921  |
| -25     | 200         | 87.1   | 87.9        | 3.328  | 67.6   | 107.4       | 2.960  | 92.1   | 82.9        | 3.485  |
| 0       | 175         | 97.7   | 77.3        | 2.961  | 82.4   | 92.6        | 2.631  | 102.8  | 72.2        | 3.093  |
| 25      | 150         | 105.4  | 69.6        | 2.544  | 91.3   | 83.7        | 2.398  | 105.4  | 69.6        | 2.701  |
| 50      | 125         | 115.9  | 59.1        | 2.203  | 105.1  | 69.9        | 2.052  | 115.1  | 59.9        | 2.332  |
| 75      | 100         | 126.1  | 48.9        | 1.860  | 117.4  | 57.6        | 1.753  | 123.0  | 52.0        | 1.983  |
| 100     | 75          | 136.4  | 38.6        | 1.521  | 129.4  | 45.6        | 1.462  | 133.7  | 41.3        | 1.606  |
| 125     | 50          | 146.9  | 28.1        | 1.172  | 142.9  | 32.1        | 1.117  | 145.1  | 29.9        | 1.211  |
| 150     | 25          | 157.2  | 17.8        | 0.8269 | 155.8  | 19.2        | 0.7947 | 157.8  | 17.2        | 0.8539 |
| H-215-2 |             | SN 004 |             |        | SN 005 |             |        | SN 006 |             |        |
| $T_a$   | $T_j - T_a$ | $T_c$  | $T_j - T_c$ | (W)    | $T_c$  | $T_j - T_c$ | (W)    | $T_c$  | $T_j - T_c$ | (W)    |
| -55     | 230         | 71.9   | 103.1       | 3.629  | 67.1   | 107.9       | 3.539  | 75.4   | 99.6        | 3.661  |
| -25     | 200         | 83.9   | 91.1        | 3.235  | 80.7   | 94.3        | 3.152  | 88.2   | 86.8        | 3.261  |
| 0       | 175         | 95.3   | 79.7        | 2.892  | 91.5   | 83.5        | 2.844  | 99.4   | 75.6        | 2.915  |
| 25      | 150         | 107.5  | 67.5        | 2.518  | 104.1  | 70.9        | 2.475  | 110.8  | 64.2        | 2.551  |
| 50      | 125         | 118.4  | 56.6        | 2.180  | 114.4  | 60.6        | 2.176  | 122.1  | 52.9        | 2.215  |
| 75      | 100         | 128.8  | 46.2        | 1.851  | 126.3  | 48.7        | 1.828  | 132.2  | 42.8        | 1.895  |
| 100     | 75          | 139.0  | 36.0        | 1.535  | 137.4  | 37.6        | 1.497  | 142.7  | 32.3        | 1.577  |
| 125     | 50          | 148.2  | 26.8        | 1.213  | 148.1  | 26.9        | 1.198  | 151.8  | 23.2        | 1.51.8 |
| 150     | 25          | 159.7  | 15.3        | 0.8869 | 159.9  | 15.1        | 0.8518 | 163.3  | 11.7        | 0.9351 |
| H-215-3 |             | SN 007 |             |        | SN 008 |             |        | SN 009 |             |        |
| $T_a$   | $T_j - T_a$ | $T_c$  | $T_j - T_c$ | (W)    | $T_c$  | $T_j - T_c$ | (W)    | $T_c$  | $T_j - T_c$ | (W)    |
| -55     | 230         | 92.3   | 82.7        | 4.188  | 78.4   | 96.6        | 4.005  | 104.5  | 70.5        | 4.251  |
| -25     | 200         | 103.5  | 71.5        | 3.688  | 90.8   | 84.2        | 3.501  | 113.2  | 61.8        | 3.773  |
| 0       | 175         | 111.8  | 63.2        | 3.277  | 102.1  | 72.9        | 3.026  | 120.7  | 54.3        | 3.366  |
| +25     | 150         | 120.9  | 54.1        | 2.850  | 112.0  | 63.0        | 2.636  | 128.1  | 46.9        | 2.905  |
| +50     | 125         | 129.2  | 45.8        | 2.447  | 119.9  | 55.1        | 2.337  | 134.5  | 40.5        | 2.532  |
| +75     | 100         | 137.4  | 37.6        | 2.063  | 130.4  | 44.6        | 1.910  | 142.1  | 32.9        | 2.100  |
| +100    | 75          | 145.5  | 29.5        | 1.684  | 138.6  | 36.4        | 1.586  | 149.0  | 26.0        | 1.703  |
| +125    | 50          | 153.7  | 21.3        | 1.292  | 148.2  | 26.8        | 1.204  | 155.7  | 19.3        | 1.321  |
| +150    | 25          | 161.9  | 13.1        | 0.918  | 157.7  | 17.3        | 0.819  | 163.2  | 11.8        | 0.917  |
| H-215-4 |             | SN 010 |             |        | SN 011 |             |        | SN 012 |             |        |
| $T_a$   | $T_j - T_a$ | $T_c$  | $T_j - T_c$ | (W)    | $T_c$  | $T_j - T_c$ | (W)    | $T_c$  | $T_j - T_c$ | (W)    |
| -55     | 230         | 84.8   | 90.2        | 3.884  | 79.0   | 96.0        | 3.951  | 76.2   | 98.8        | 4.045  |
| -25     | 200         | 96.5   | 79.5        | 3.450  | 91.3   | 83.7        | 3.536  | 88.9   | 86.1        | 3.606  |
| 0       | 175         | 106.4  | 68.6        | 3.076  | 102.5  | 72.5        | 3.116  | 99.3   | 75.7        | 3.230  |
| 25      | 150         | 116.3  | 58.7        | 2.695  | 113.3  | 61.7        | 2.744  | 110.9  | 64.1        | 2.817  |
| 50      | 125         | 125.5  | 49.5        | 2.326  | 123.1  | 51.9        | 2.387  | 121.9  | 53.1        | 2.439  |
| 75      | 100         | 135.1  | 39.9        | 1.963  | 131.8  | 43.2        | 2.088  | 131.6  | 43.4        | 2.077  |
| 100     | 75          | 144.1  | 30.9        | 1.625  | 141.9  | 33.1        | 1.719  | 141.3  | 33.7        | 1.736  |
| 125     | 50          | 152.8  | 22.2        | 1.266  | 152.9  | 22.1        | 1.331  | 151.9  | 23.1        | 1.350  |
| 150     | 25          | 163.0  | 12.0        | 0.927  | 162.8  | 12.2        | 0.971  | 162.7  | 12.3        | 0.975  |

| H 216-1B |             | SN 004 |             |        |        |             |        |
|----------|-------------|--------|-------------|--------|--------|-------------|--------|
| $T_a$    | $T_j - T_a$ | $T_c$  | $T_j - T_c$ | (W)    |        |             |        |
| -55      | 230         | 24.1   | 150.1       | 12.144 |        |             |        |
| -25      | 200         | 43.0   | 132.0       | 10.283 |        |             |        |
| 0        | 175         | 59.0   | 116.0       | 8.951  |        |             |        |
| 25       | 150         | 77.0   | 98.0        | 7.604  |        |             |        |
| 50       | 125         | 92.4   | 82.6        | 6.406  |        |             |        |
| 75       | 100         | 107.6  | 67.4        | 5.187  |        |             |        |
| 100      | 75          | 122.5  | 52.5        | 3.962  |        |             |        |
| 125      | 50          | 138.1  | 36.9        | 2.817  |        |             |        |
| 150      | 25          | 152.6  | 22.4        | 1.636  |        |             |        |
| H 216-2A |             | SN 005 |             |        | SN 006 |             |        |
| $T_a$    | $T_a - T_j$ | $T_c$  | $T_j - T_c$ | (W)    | $T_c$  | $T_j - T_c$ | (W)    |
| -55      | 230         | 35.0   | 140.0       | 9.422  | 14.7   | 160.3       | 10.186 |
| -25      | 200         | 50.3   | 124.7       | 8.411  | 33.1   | 141.9       | 9.252  |
| 0        | 175         | 67.2   | 107.8       | 7.505  | 50.4   | 124.6       | 8.266  |
| 25       | 150         | 84.1   | 90.9        | 6.525  | 69.6   | 105.4       | 7.016  |
| 50       | 125         | 97.9   | 77.1        | 5.648  | 87.3   | 87.7        | 6.003  |
| 75       | 100         | 112.3  | 62.7        | 4.728  | 104.8  | 70.2        | 4.943  |
| 100      | 75          | 126.1  | 48.9        | 3.790  | 122.3  | 52.7        | 3.889  |
| 125      | 50          | 142.5  | 32.5        | 2.863  | 139.3  | 35.7        | 2.946  |
| 150      | 25          | 157.2  | 17.8        | 1.941  | 153.6  | 21.4        | 1.885  |
| H 216-2B |             | SN 007 |             |        | SN 008 |             |        |
| $T_a$    | $T_j - T_a$ | $T_c$  | $T_j - T_c$ | (W)    | $T_c$  | $T_j - T_c$ | (W)    |
| -55      | 230         | 16.8   | 158.2       | 10.575 | 46.2   | 128.8       | 8.549  |
| -25      | 200         | 37.3   | 137.7       | 9.375  | 63.9   | 111.1       | 7.575  |
| 0        | 175         | 55.4   | 119.6       | 8.299  | 79.0   | 96.0        | 6.722  |
| 25       | 150         | 72.7   | 102.3       | 7.222  | 93.9   | 81.1        | 5.880  |
| 50       | 125         | 89.2   | 85.8        | 6.175  | 106.4  | 68.6        | 5.122  |
| 75       | 100         | 106.1  | 68.9        | 5.124  | 120.5  | 54.5        | 4.328  |
| 100      | 75          | 122.0  | 53.0        | 4.063  | 133.3  | 41.7        | 3.558  |
| 125      | 50          | 139.3  | 35.7        | 3.045  | 148.0  | 27.0        | 2.790  |
| 150      | 25          | 154.8  | 20.2        | 1.868  | 160.5  | 14.5        | 1.901  |



| H 216-3A |             | SN 009 |             |        | SN 010 |             |        |
|----------|-------------|--------|-------------|--------|--------|-------------|--------|
| $T_a$    | $T_j - T_a$ | $T_c$  | $T_j - T_c$ | (W)    | $T_c$  | $T_j - T_c$ | (W)    |
| -55      | 230         | 36.9   | 138.1       | 13.651 | 34.4   | 140.6       | 13.416 |
| -25      | 200         | 53.5   | 121.5       | 12.143 | 51.8   | 123.2       | 11.784 |
| 0        | 175         | 68.6   | 106.4       | 10.722 | 65.7   | 109.3       | 10.406 |
| 25       | 150         | 85.7   | 89.3        | 9.156  | 82.1   | 92.9        | 8.752  |
| 50       | 125         | 100.3  | 74.7        | 7.781  | 96.9   | 78.1        | 7.278  |
| 75       | 100         | 115.1  | 59.9        | 6.352  | 110.5  | 64.5        | 5.873  |
| 100      | 75          | 129.2  | 45.8        | 4.970  | 124.3  | 50.7        | 4.430  |
| 125      | 50          | 143.5  | 31.5        | 3.584  | 138.5  | 36.5        | 2.984  |
| 150      | 25          | 157.7  | 17.3        | 2.174  | 152.2  | 22.8        | 1.555  |
| H 216-3B |             | SN 011 |             |        | SN 012 |             |        |
| $T_a$    | $T_j - T_a$ | $T_c$  | $T_j - T_c$ | (W)    | $T_c$  | $T_j - T_c$ | (W)    |
| -55      | 230         | 46.1   | 128.9       | 9.557  | 27.9   | 147.1       | 11.986 |
| -25      | 200         | 62.5   | 112.5       | 8.587  | 40.3   | 134.7       | 10.902 |
| 0        | 175         | 76.5   | 98.5        | 7.746  | 57.1   | 11.9        | 9.760  |
| 25       | 150         | 91.2   | 83.8        | 6.706  | 76.0   | 99.0        | 8.454  |
| 50       | 125         | 105.2  | 69.8        | 5.797  | 93.0   | 82.0        | 7.209  |
| 75       | 100         | 118.2  | 56.8        | 4.859  | 110.0  | 65.0        | 5.943  |
| 100      | 75          | 131.1  | 43.9        | 3.867  | 126.2  | 48.8        | 4.689  |
| 125      | 50          | 144.2  | 30.8        | 3.854  | 142.2  | 32.8        | 3.435  |
| 150      | 25          | 157.1  | 17.9        | 1.804  | 157.7  | 17.3        | 2.160  |
| H 216-4A |             | SN 013 |             |        | SN 014 |             |        |
| $T_a$    | $T_j - T_a$ | $T_c$  | $T_j - T_c$ | (W)    | $T_c$  | $T_j - T_c$ | (W)    |
| -55      | 230         | 30.8   | 144.2       | 11.046 | 44.6   | 130.4       | 9.359  |
| -25      | 200         | 48.9   | 126.1       | 9.815  | 60.9   | 114.1       | 8.296  |
| 0        | 175         | 65.2   | 109.8       | 8.681  | 74.4   | 100.6       | 7.388  |
| 25       | 150         | 80.4   | 94.6        | 7.577  | 89.4   | 85.6        | 6.411  |
| 50       | 125         | 95.5   | 79.5        | 6.482  | 102.9  | 72.1        | 5.547  |
| 75       | 100         | 110.4  | 64.6        | 5.355  | 116.4  | 58.6        | 4.605  |
| 100      | 75          | 124.8  | 50.2        | 4.217  | 129.4  | 45.6        | 3.670  |
| 125      | 50          | 139.8  | 35.2        | 3.033  | 142.9  | 32.1        | 2.684  |
| 150      | 25          | 154.7  | 20.3        | 1.890  | 156.4  | 18.6        | 1.739  |



| H 216-4B |             | SN 015 |             |        |        |             |       |
|----------|-------------|--------|-------------|--------|--------|-------------|-------|
| $T_a$    | $T_j - T_a$ | $T_c$  | $T_j - T_c$ | (W)    |        |             |       |
| -55      | 230         | 31.7   | 143.3       | 11.389 |        |             |       |
| -25      | 200         | 42.1   | 132.9       | 10.017 |        |             |       |
| 0        | 175         | 57.9   | 117.1       | 8.896  |        |             |       |
| 25       | 150         | 76.4   | 98.6        | 7.690  |        |             |       |
| 50       | 125         | 92.7   | 82.3        | 6.579  |        |             |       |
| 75       | 100         | 109.4  | 65.6        | 5.437  |        |             |       |
| 100      | 75          | 125.8  | 49.2        | 4.347  |        |             |       |
| 125      | 50          | 142.3  | 32.7        | 3.193  |        |             |       |
| 150      | 25          | 157.7  | 17.3        | 2.120  |        |             |       |
| H 217-1A |             | SN 001 |             |        | SN 002 |             |       |
| $T_a$    | $T_j - T_a$ | $T_c$  | $T_j - T_c$ | (W)    | $T_c$  | $T_j - T_c$ | (W)   |
| -55      | 230         | 21.1   | 153.9       | 4.891  | 19.4   | 155.6       | 7.085 |
| -25      | 200         | 44.2   | 130.8       | 4.324  | 40.1   | 134.9       | 6.256 |
| 0        | 175         | 52.1   | 122.9       | 4.158  | 57.1   | 117.9       | 5.490 |
| 25       | 150         | 70.8   | 104.2       | 3.636  | 74.6   | 100.4       | 4.738 |
| 50       | 125         | 89.2   | 85.80       | 3.136  | 89.1   | 85.9        | 3.921 |
| 75       | 100         | 105.8  | 69.2        | 2.598  | 107.2  | 67.8        | 3.346 |
| 100      | 75          | 121.0  | 54.0        | 2.110  | 123.6  | 51.4        | 2.596 |
| 125      | 50          | 137.3  | 37.7        | 1.566  | 139.6  | 35.4        | 1.901 |
| 150      | 25          | 154.2  | 20.8        | 0.977  | 156.4  | 18.6        | 1.148 |
| H 217-1B |             | SN 003 |             |        | SN 004 |             |       |
| $T_a$    | $T_j - T_a$ | $T_c$  | $T_j - T_c$ | (W)    | $T_c$  | $T_j - T_c$ | (W)   |
| -55      | 230         | 10.2   | 164.8       |        | 18.0   | 157.0       | 5.822 |
| -25      | 200         | 33.6   | 141.4       |        | 39.2   | 135.8       | 5.227 |
| 0        | 175         | 57.6   | 117.4       |        | 56.8   | 118.2       | 4.640 |
| 25       | 150         | 76.9   | 98.1        |        | 74.8   | 100.2       | 4.120 |
| 50       | 125         | 93.6   | 81.4        |        | 92.6   | 82.4        | 3.522 |
| 75       | 100         | 108.7  | 66.3        |        | 108.9  | 66.1        | 2.955 |
| 100      | 75          |        |             |        | 125.0  | 50.0        | 2.396 |
| 125      | 25          | 155.7  | 19.3        |        | 142.2  | 32.8        | 1.808 |
| 150      | 25          | 155.7  | 19.3        |        | 158.0  | 17.0        | 1.216 |

| H 217-2A |             | SN 005 |             |       | SN 006 |             |       |
|----------|-------------|--------|-------------|-------|--------|-------------|-------|
| $T_a$    | $T_j - T_a$ | $T_c$  | $T_j - T_c$ | (W)   | $T_c$  | $T_j - T_c$ | (W)   |
| -55      | 230         | 23.3   | 151.7       | 4.289 | 17.5   | 157.5       | 5.609 |
| -25      | 200         | 42.8   | 132.2       | 3.814 | 37.6   | 137.4       | 4.934 |
| 0        | 175         | 59.6   | 115.4       | 3.399 | 54.0   | 121.0       | 4.367 |
| 25       | 150         | 77.0   | 98.00       | 2.980 | 71.5   | 103.5       | 3.747 |
| 50       | 125         | 94.1   | 80.9        | 2.556 | 88.3   | 86.7        | 3.164 |
| 75       | 100         | 109.8  | 65.2        | 2.178 | 104.8  | 70.2        | 2.596 |
| 100      | 75          | 125.9  | 49.1        | 1.773 | 121.8  | 53.2        | 2.022 |
| 125      | 50          | 142.6  | 32.4        | 1.394 | 138.6  | 36.4        | 1.507 |
| 150      | 25          | 158.4  | 16.6        | 0.967 | 155.2  | 19.8        | 0.905 |
| H 217-2B |             | SN 007 |             |       | SN 008 |             |       |
| $T_a$    | $T_j - T_a$ | $T_c$  | $T_j - T_c$ | (W)   | $T_c$  | $T_j - T_c$ | (W)   |
| -55      | 230         | 12.4   | 162.6       | 5.344 | 18.8   | 156.2       | 4.978 |
| -25      | 200         | 34.1   | 140.9       | 4.823 | 28.7   | 136.3       | 4.394 |
| 0        | 175         | 53.1   | 121.9       | 4.342 | 55.0   | 120.0       | 3.901 |
| 25       | 150         | 69.1   | 105.9       | 3.810 | 71.3   | 103.7       | 3.418 |
| 50       | 125         | 86.8   | 88.2        | 3.257 | 88.0   | 87.0        | 2.920 |
| 75       | 100         | 104.0  | 71.0        | 2.705 | 104.5  | 70.5        | 2.411 |
| 100      | 75          | 120.8  | 54.2        | 2.161 | 121.2  | 53.8        | 1.877 |
| 125      | 50          | 139.1  | 35.9        | 1.574 | 138.1  | 36.9        | 1.404 |
| 150      | 25          | 155.8  | 19.2        | 1.081 | 155.1  | 19.9        | 0.903 |
| H 217-3A |             | SN 009 |             |       | SN 010 |             |       |
| $T_a$    | $T_j - T_a$ | $T_c$  | $T_j - T_c$ | (W)   | $T_c$  | $T_j - T_c$ | (W)   |
| -55      | 230         | 52.1   | 122.9       | 5.809 |        |             |       |
| -25      | 200         | 68.0   | 107.0       | 5.056 | 37.4   | 137.6       | 5.866 |
| 0        | 175         | 81.9   | 93.1        | 4.454 | 55.9   | 119.1       | 5.382 |
| 25       | 150         | 94.7   | 80.3        | 3.888 | 74.4   | 100.6       | 4.817 |
| 50       | 125         | 107.5  | 67.5        | 3.309 | 91.8   | 83.2        | 4.160 |
| 75       | 100         | 121.7  | 53.3        | 2.722 | 108.3  | 66.7        | 3.450 |
| 100      | 75          | 133.8  | 41.2        | 2.173 | 125.7  | 49.3        | 2.875 |
| 125      | 50          | 146.2  | 28.8        | 1.558 | 141.2  | 33.8        | 2.018 |
| 150      | 25          | 158.7  | 16.3        | 0.999 | 155.9  | 19.1        | 1.154 |

| H 217-3B |             | SN 0011 |             |       | SN 012 |             |        |
|----------|-------------|---------|-------------|-------|--------|-------------|--------|
| $T_a$    | $T_j - T_a$ | $T_c$   | $T_j - T_c$ | (W)   | $T_c$  | $T_j - T_c$ | (W)    |
| -55      | 230         | 52.9    | 122.1       | 6.306 | 21.6   | 153.4       | 6.306  |
| -25      | 200         | 70.0    | 105.0       | 5.584 | 42.4   | 132.6       | 5.584  |
| 0        | 175         | 84.2    | 90.8        | 4.997 | 58.4   | 116.6       | 4.997  |
| 25       | 150         | 98.1    | 76.9        | 4.357 | 75.1   | 99.9        | 4.357  |
| 50       | 125         | 111.2   | 63.8        | 3.756 | 91.9   | 83.1        | 3.756  |
| 75       | 100         | 124.0   | 51.0        | 3.165 | 108.0  | 67.0        | 3.165  |
| 100      | 75          | 136.6   | 38.4        | 2.493 | 128.6  | 46.0        | 2.493  |
| 125      | 50          | 149.7   | 25.3        | 1.849 | 139.6  | 35.4        | 1.849  |
| 150      | 25          | 162.3   | 12.7        | 1.205 | 155.2  | 19.8        | 1.205  |
| H 217-4A |             | SN 013  |             |       | SN 014 |             |        |
| $T_a$    | $T_j - T_a$ | $T_c$   | $T_j - T_c$ | (W)   | $T_c$  | $T_j - T_c$ | (W)    |
| -55      | 230         | 37.2    | 137.8       | 5.431 | 16.6   | 158.4       | 6.059  |
| -25      | 200         | 36.5    | 138.5       | 4.878 | 36.1   | 138.9       | 5.458  |
| 0        | 175         | 70.2    | 104.8       | 4.380 | 53.3   | 121.7       | 4.793  |
| 25       | 150         | 86.8    | 88.20       | 3.822 | 70.2   | 104.8       | 4.146  |
| 50       | 125         | 101.8   | 73.2        | 3.286 | 87.1   | 87.9        | 3.501  |
| 75       | 100         | 115.7   | 59.3        | 2.763 | 103.7  | 71.3        | 2.816  |
| 100      | 75          | 129.4   | 45.6        | 2.232 | 120.8  | 54.2        | 2.176  |
| 125      | 50          | 144.0   | 31.0        | 1.667 | 137.6  | 37.4        | 11.499 |
| 150      | 25          | 158.4   | 16.6        | 1.113 | 153.8  | 21.2        | 0.856  |
| H 217-4B |             | SN 015  |             |       |        |             |        |
| $T_a$    | $T_j - T_a$ | $T_c$   | $T_j - T_c$ | (W)   |        |             |        |
| -55      | 230         | 11.0    | 164.0       | 6.205 |        |             |        |
| -25      | 200         | 35.2    | 139.8       | 5.525 |        |             |        |
| 0        | 175         | 53.4    | 121.6       | 4.834 |        |             |        |
| 25       | 150         | 71.8    | 103.2       | 4.181 |        |             |        |
| 50       | 125         | 89.6    | 85.4        | 3.448 |        |             |        |
| 75       | 100         | 107.7   | 67.3        | 2.753 |        |             |        |
| 100      | 75          | 124.7   | 50.3        | 2.131 |        |             |        |
| 125      | 50          | 140.8   | 34.2        | 1.519 |        |             |        |
| 150      | 25          | 156.2   | 18.1        | 0.959 |        |             |        |



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